

# MODELOWANIE ZATRUĆ W BLOKU BERYLOWYM

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**BERYLLIUM POISONING MODEL DEVELOPMENT AND EXPERIMENTAL  
VALIDATION IN RESEARCH REACTORS WITH EXPLOITATION IN MARIA  
AND JULES-HOROVITZ REACTORS**



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Praca wykonana w ramach projektu BENICE

# Presentation overview

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- Theoretical background
- Codes and methods
- Results
- Summary
- What's next?

# Some theory...

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MARIA :

- pool type reactor
- power of 20-30 MWth
- moderated with water and beryllium
- $3 \cdot 10^{14} \text{ n/cm}^2 \cdot \text{s}$
- fuel: CERCA LEU, 19.75% enriched

**A**

141.4 ± 0.26

141.4 ± 0.26

**B**

116.5 ± 0.26

116.5 ± 0.26

**C-C**

127.8 ± 0.26

127.8 ± 0.26

1642 ± 2.0

1100 ± 2.0

550 ± 1.0

95

min 0.75

1602<sup>+1</sup><sub>-0.3</sub>

100

45

**Widok "L"**

60 ± 0.4

10

10

60

**A-A (1:1)**

**B-B (1:1)**

1. Rury paliwowe

2. Prowadnica rur paliwowych

3. Rura rozdzielająca

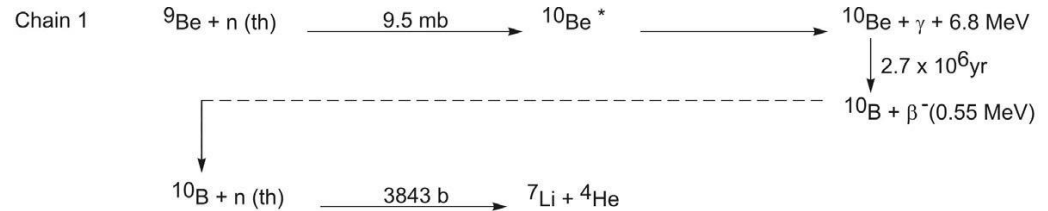
4. Końcówka górna

5. Końcówka zewnętrzna

6. Końcówka dolna

7. Żebra dystansujące

# Poisoning

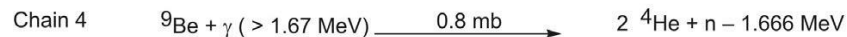
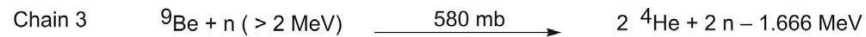
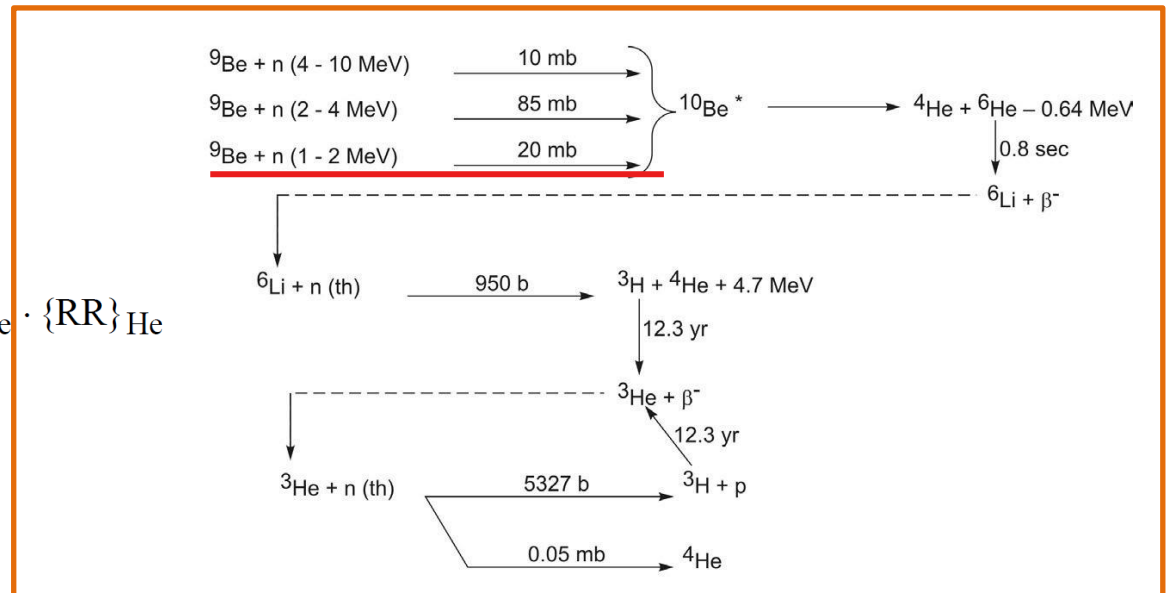


$$\frac{dN_{\text{Be}}}{dt} = -N_{\text{Be}} \cdot \{\text{RR}\}_{\text{Be}}$$

$$\frac{dN_{\text{L}}}{dt} = N_{\text{Be}} \cdot \{\text{RR}\}_{\text{Be}} - N_{\text{L}} \cdot \{\text{RR}\}_{\text{L}}$$

$$\frac{dN_{\text{T}}}{dt} = N_{\text{L}} \cdot \{\text{RR}\}_{\text{L}} - \lambda_{\text{T}} \cdot N_{\text{T}} + N_{\text{He}} \cdot \{\text{RR}\}_{\text{He}}$$

$$\frac{dN_{\text{He}}}{dt} = \lambda_{\text{T}} \cdot N_{\text{T}} - N_{\text{He}} \cdot \{\text{RR}\}_{\text{He}}$$



# Codes and methods

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## TRANSPORT CODE

- APOLLO2 (CEA France) :
  - CP method; CEA2005 libraries v10.4; XMASS 172 group structure and Pij solver.
  - MOC method; SHEM 281-group energy mesh

## MONTE CARLO

- TRIPOLI4 (CEA France)
- SERPENT 2.1.23 (VVT Finland)
- MCNP (LANL USA)

# Codes and methods

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## APOLLO2

- Collision Probability Method and Method of Characteristics
- 172 and 281 energy group library
- self-shielding calculations
- various energy cutting ( 69 groups and no cutting)
- beryllium depletion in calculations
- steady state calculation
- burnup calculations
- two types of calculation cell considered

# Codes and methods

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## SERPENT

- cold operating conditions
- burnup with 3 schemes
- cumulative burnup steps, outage calculated at the end
- cumulative burnup steps, outage calculated after each cycle
- time steps, outage calculated after each cycle

## TRIPOLI4

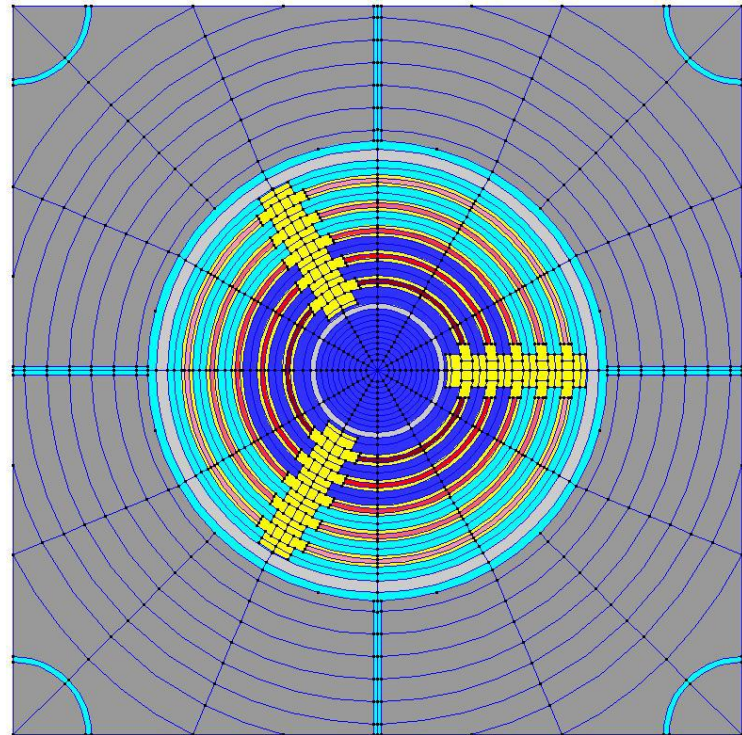
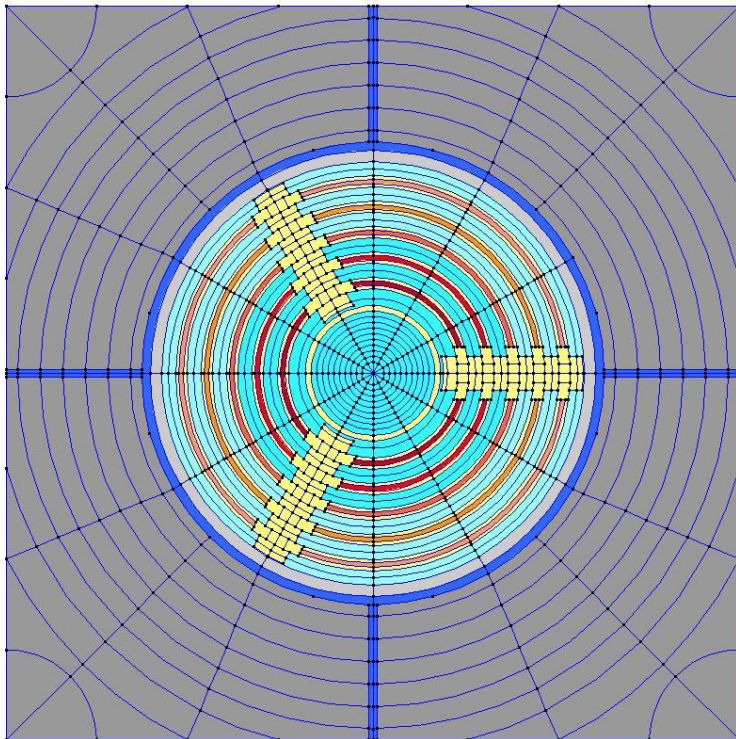
- cold operating conditions



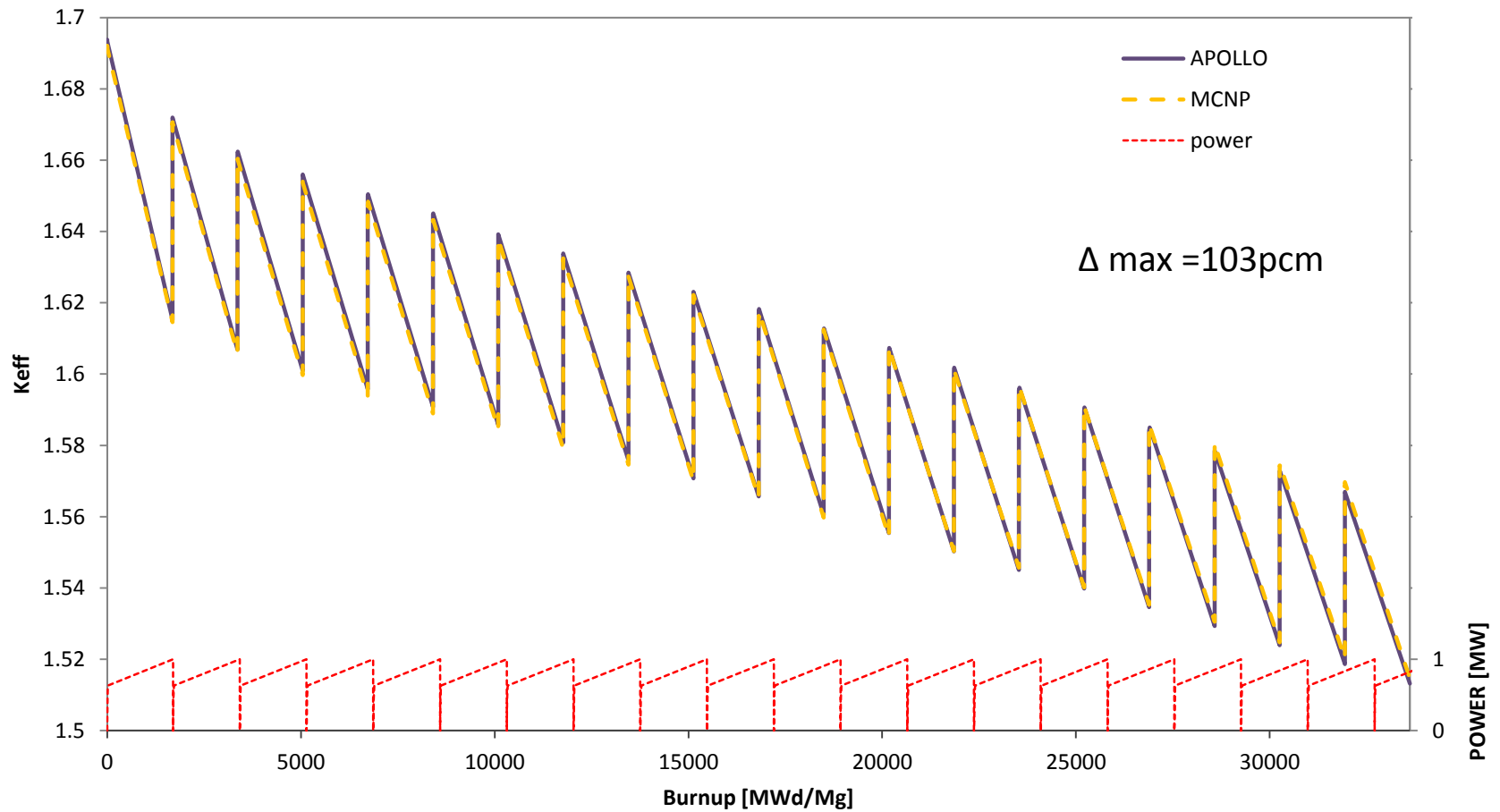
# Codes and methods

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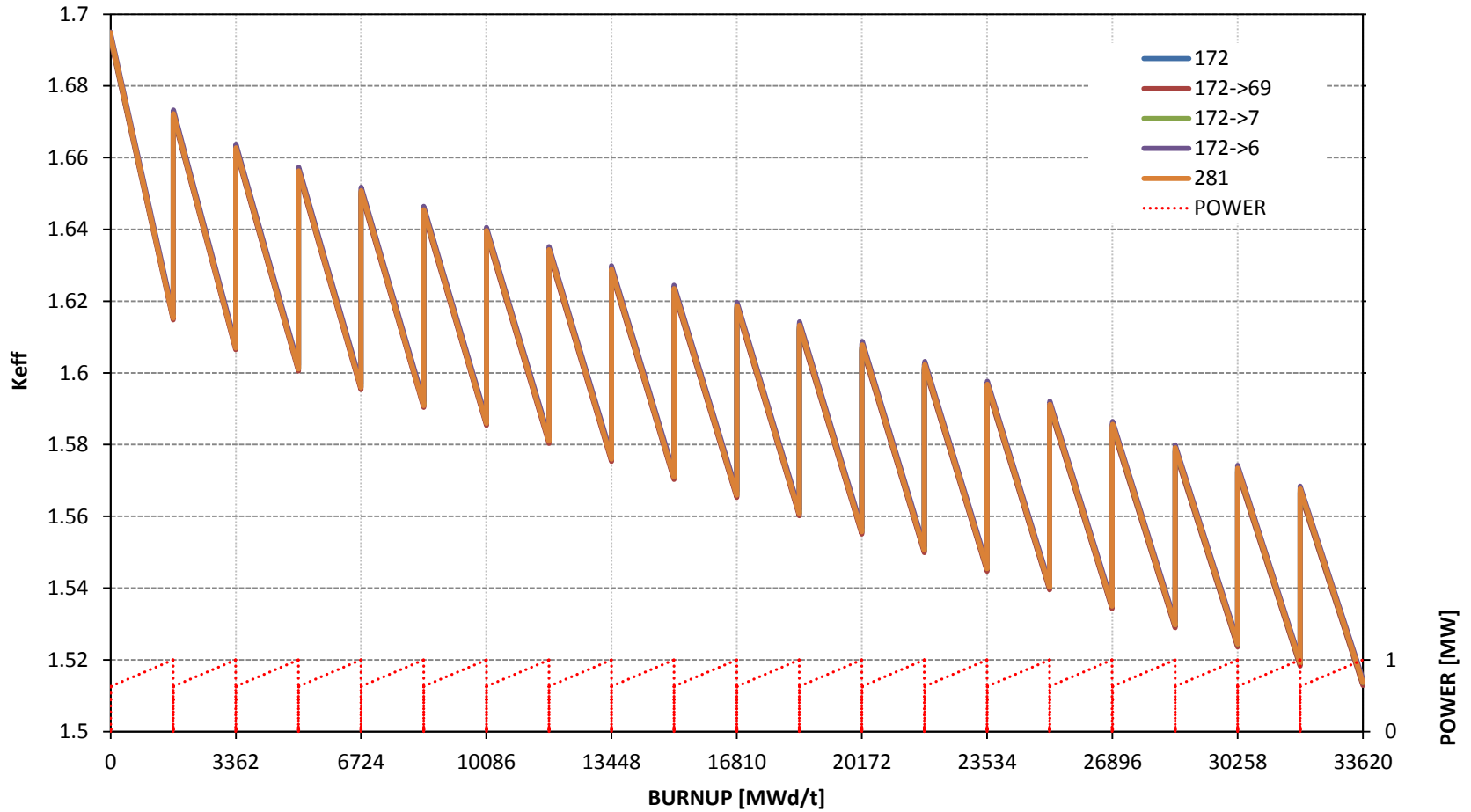
## GEOMETRY



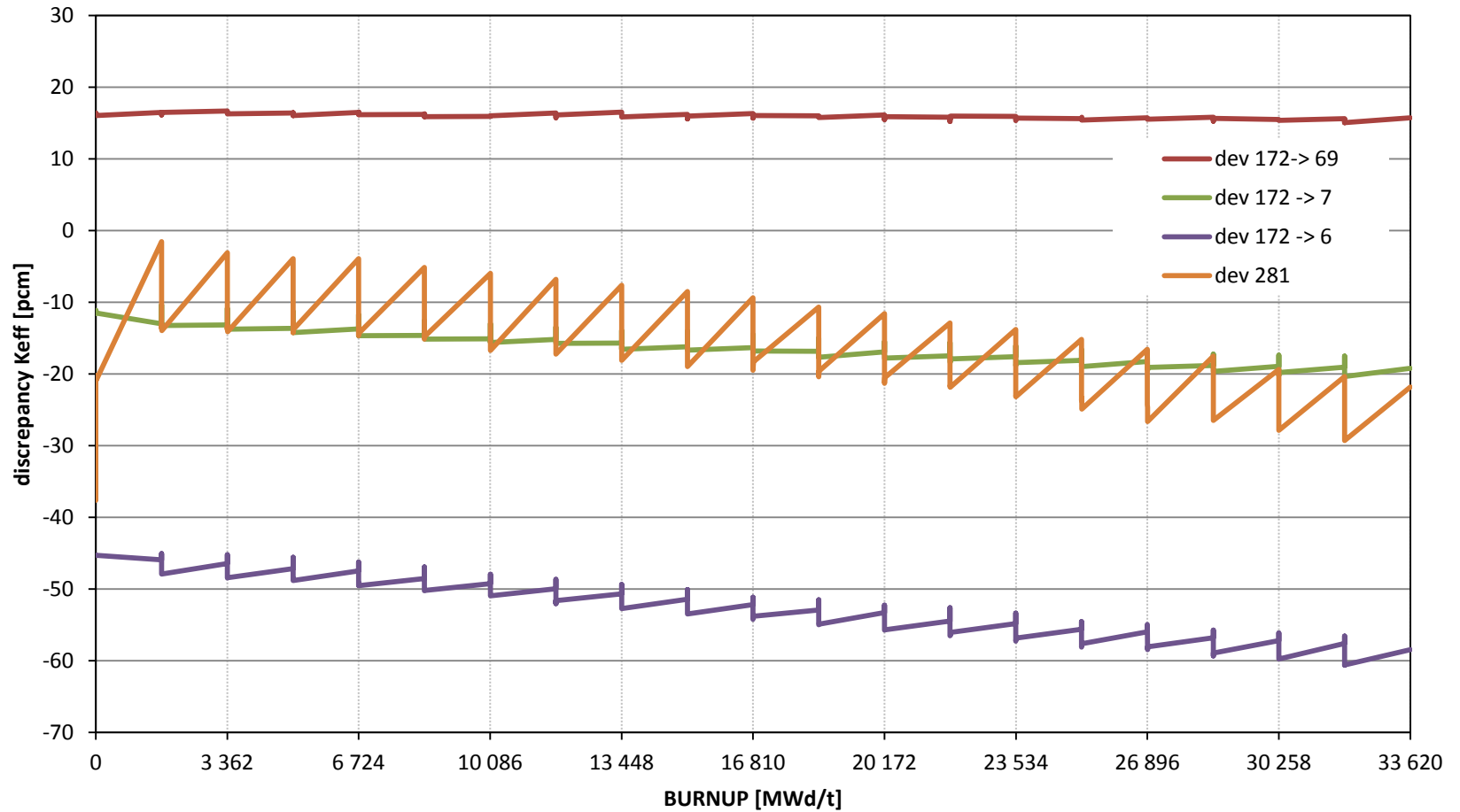
# RESULTS



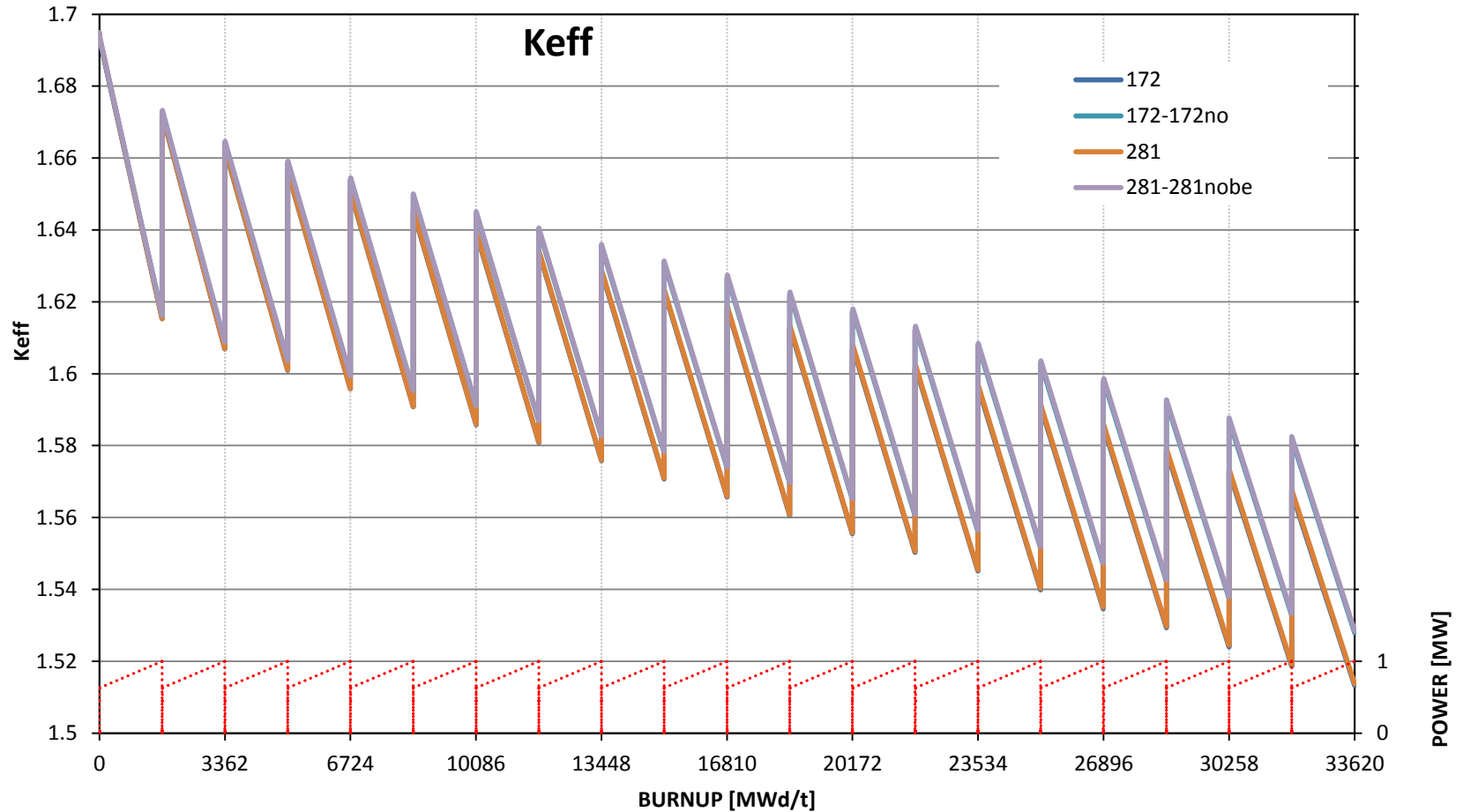
# RESULTS



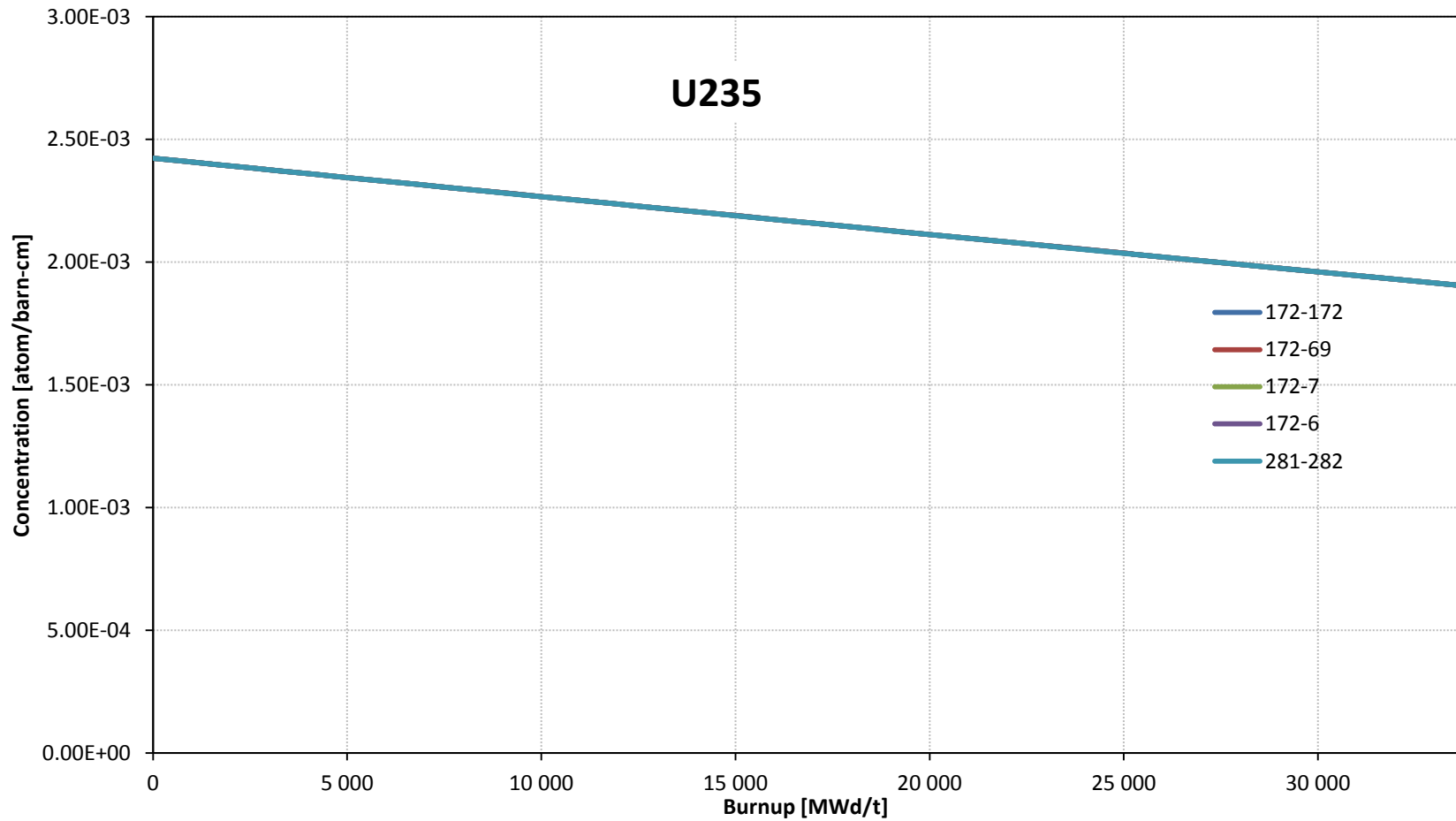
# RESULTS



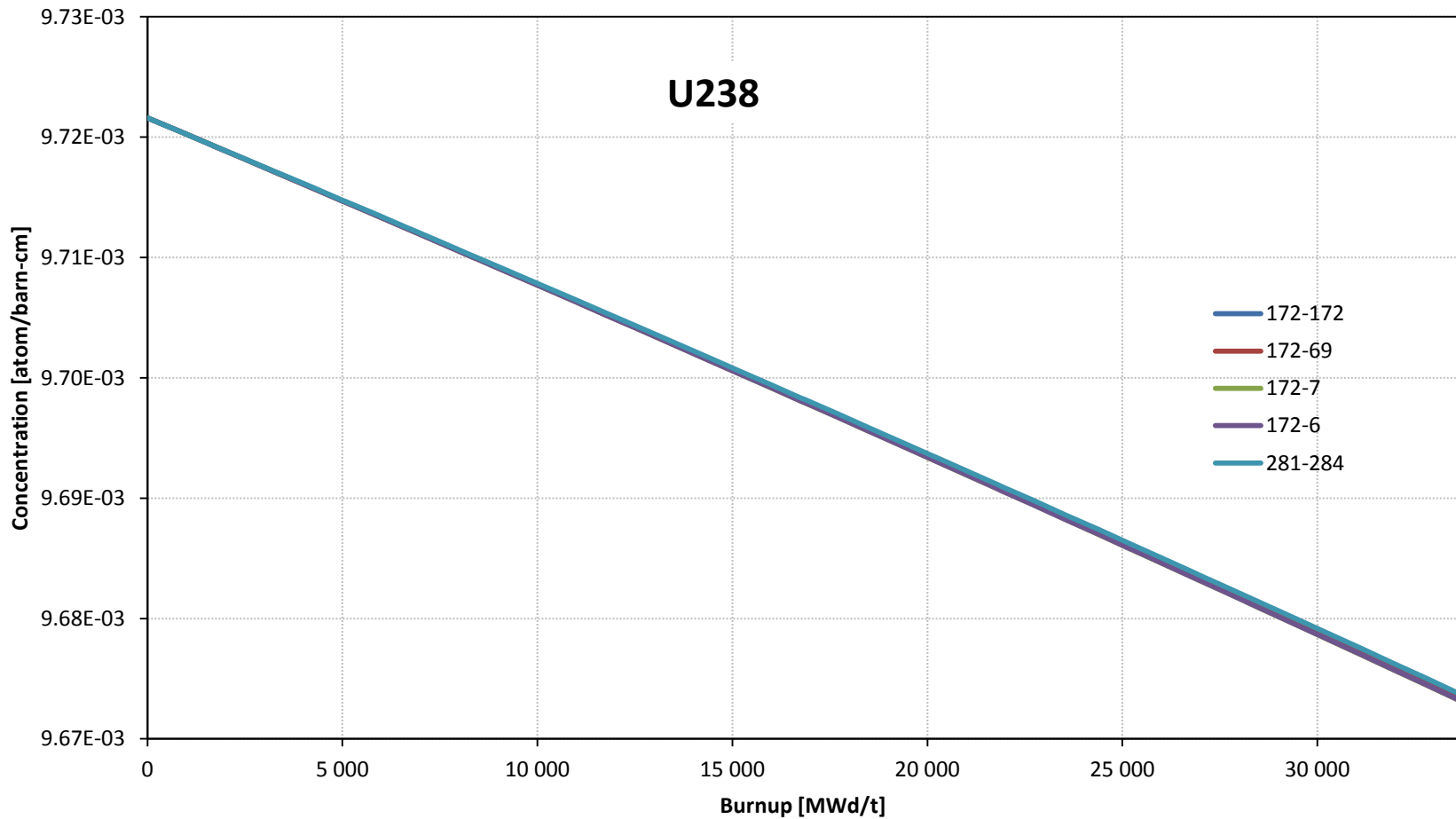
# RESULTS



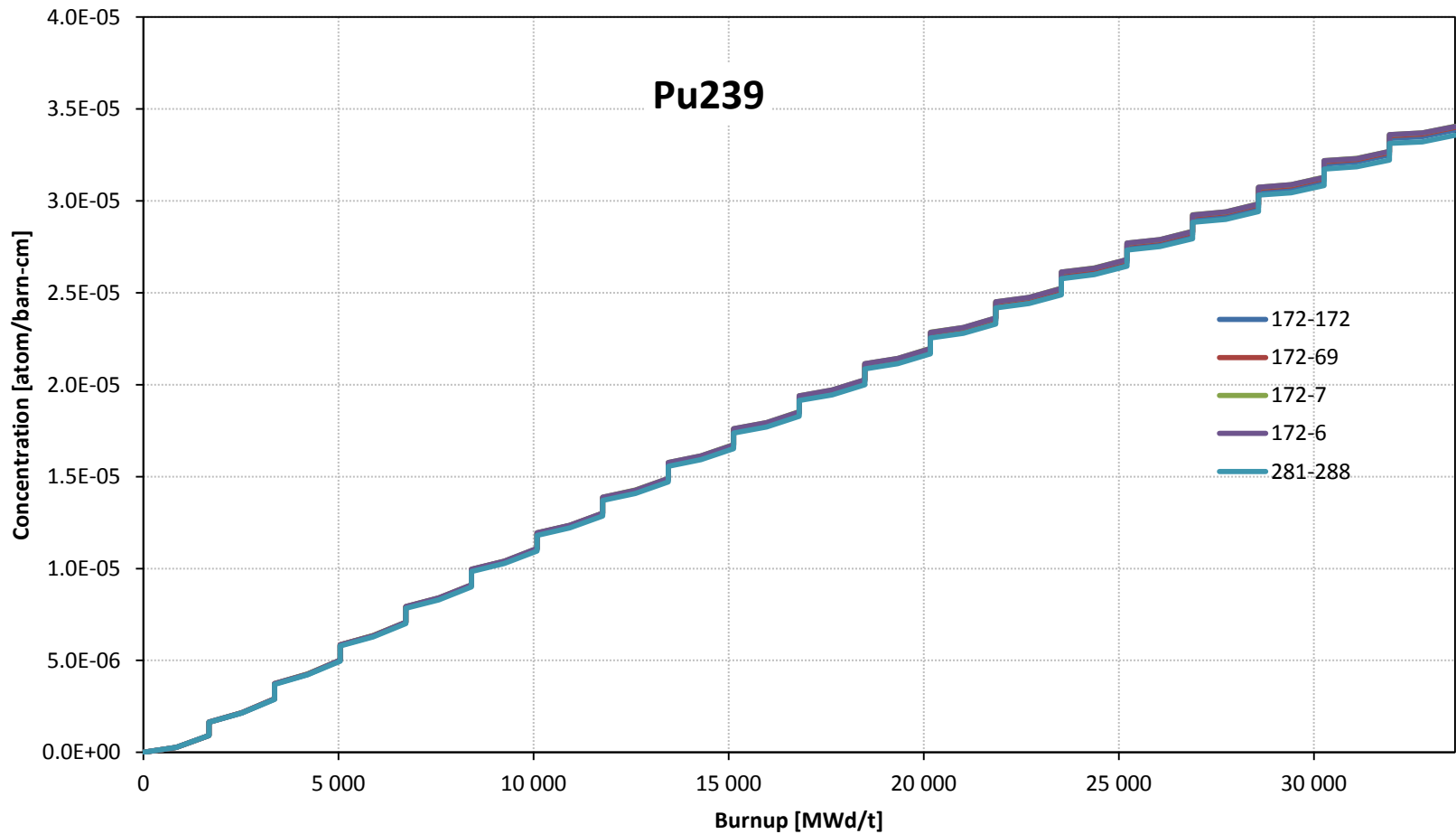
# RESULTS



# RESULTS

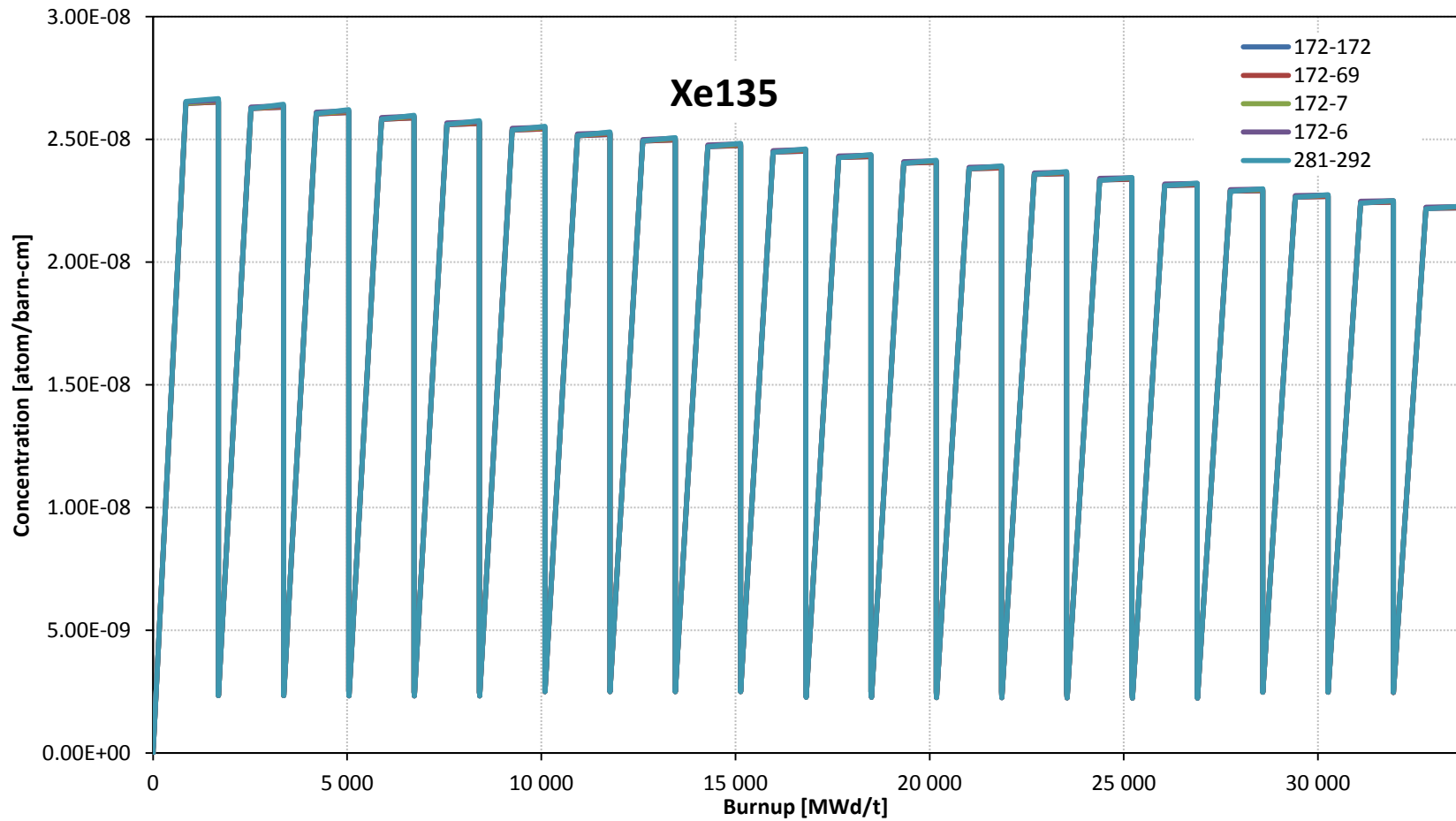


# RESULTS

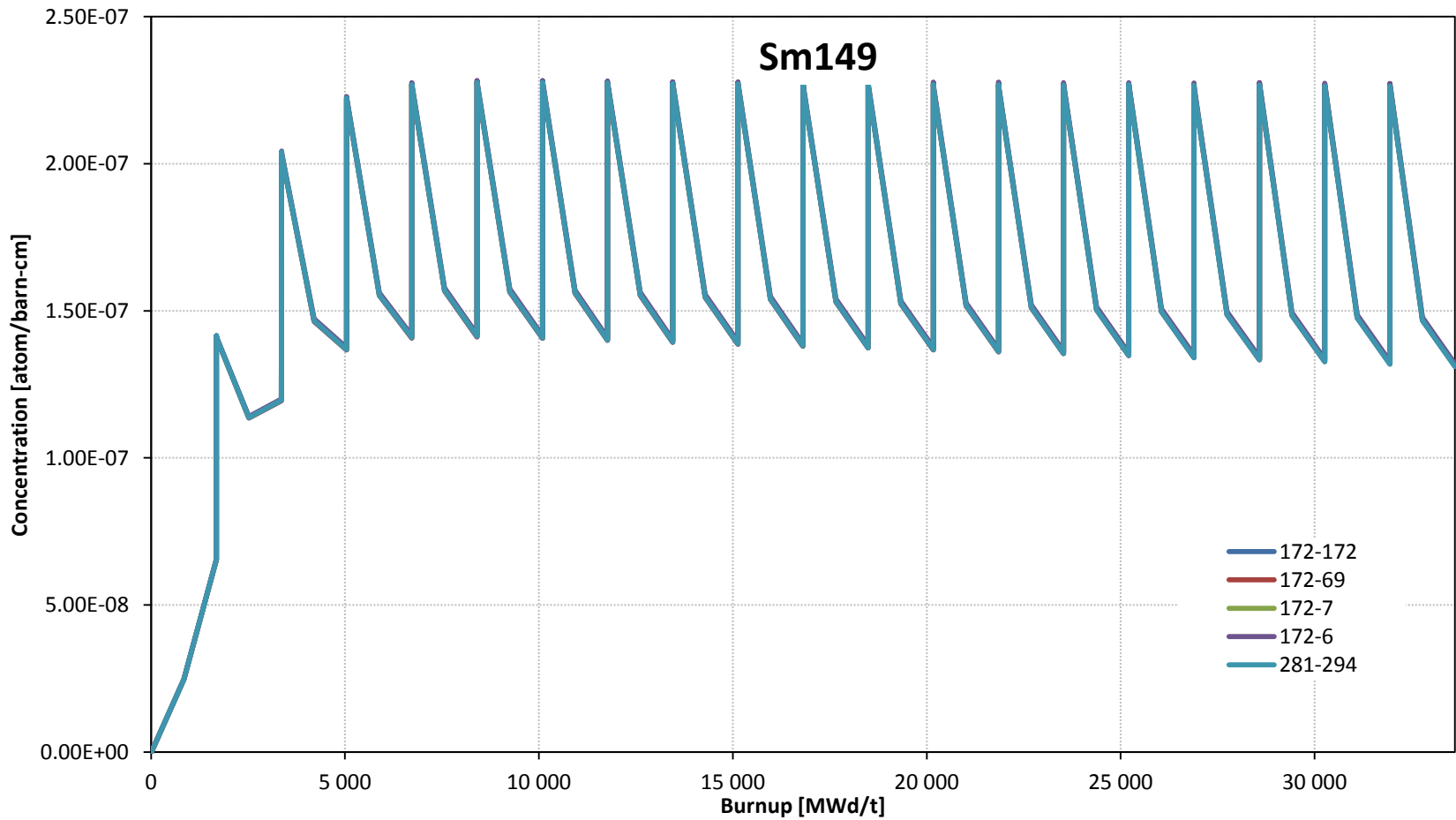




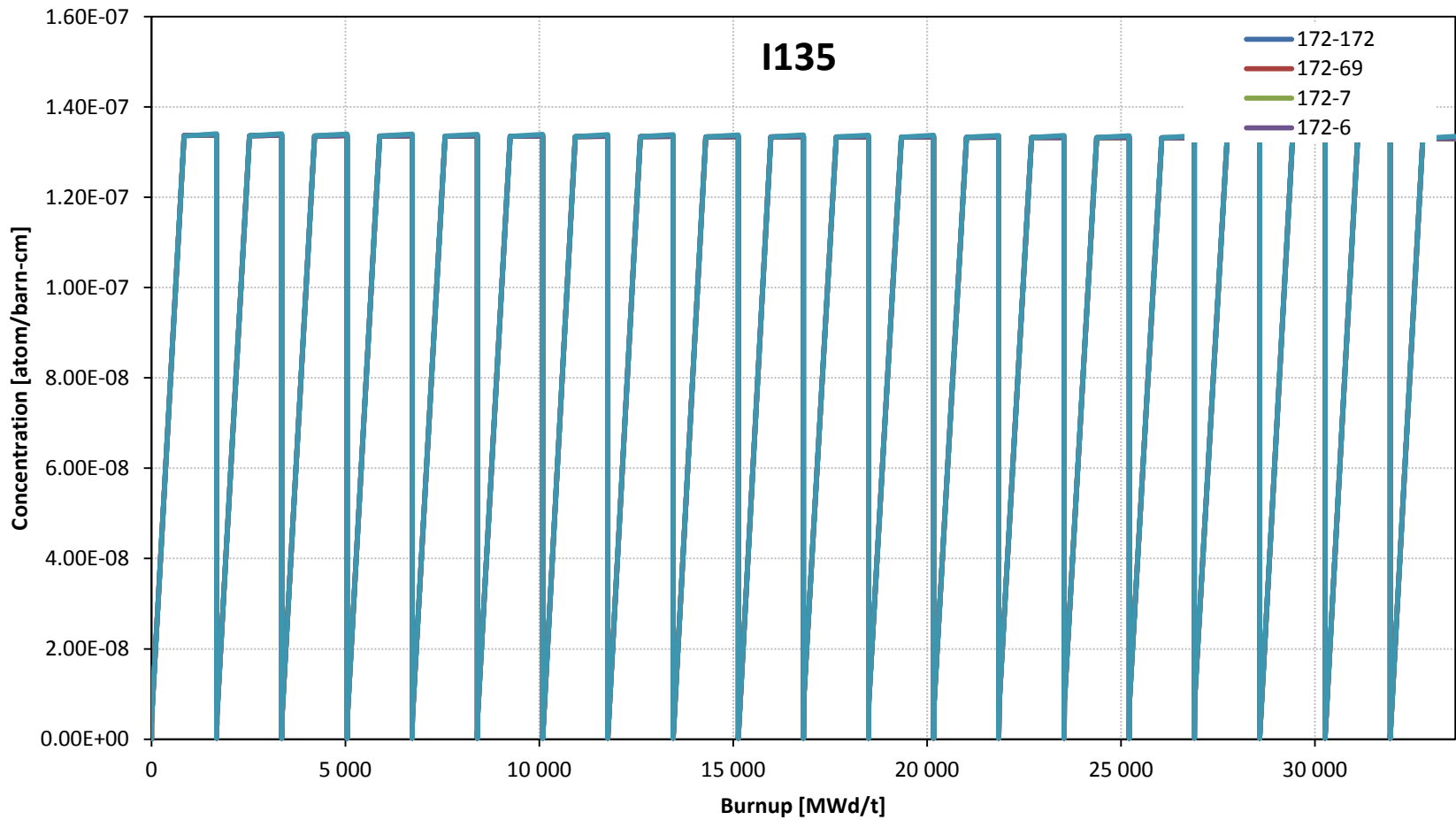
# RESULTS



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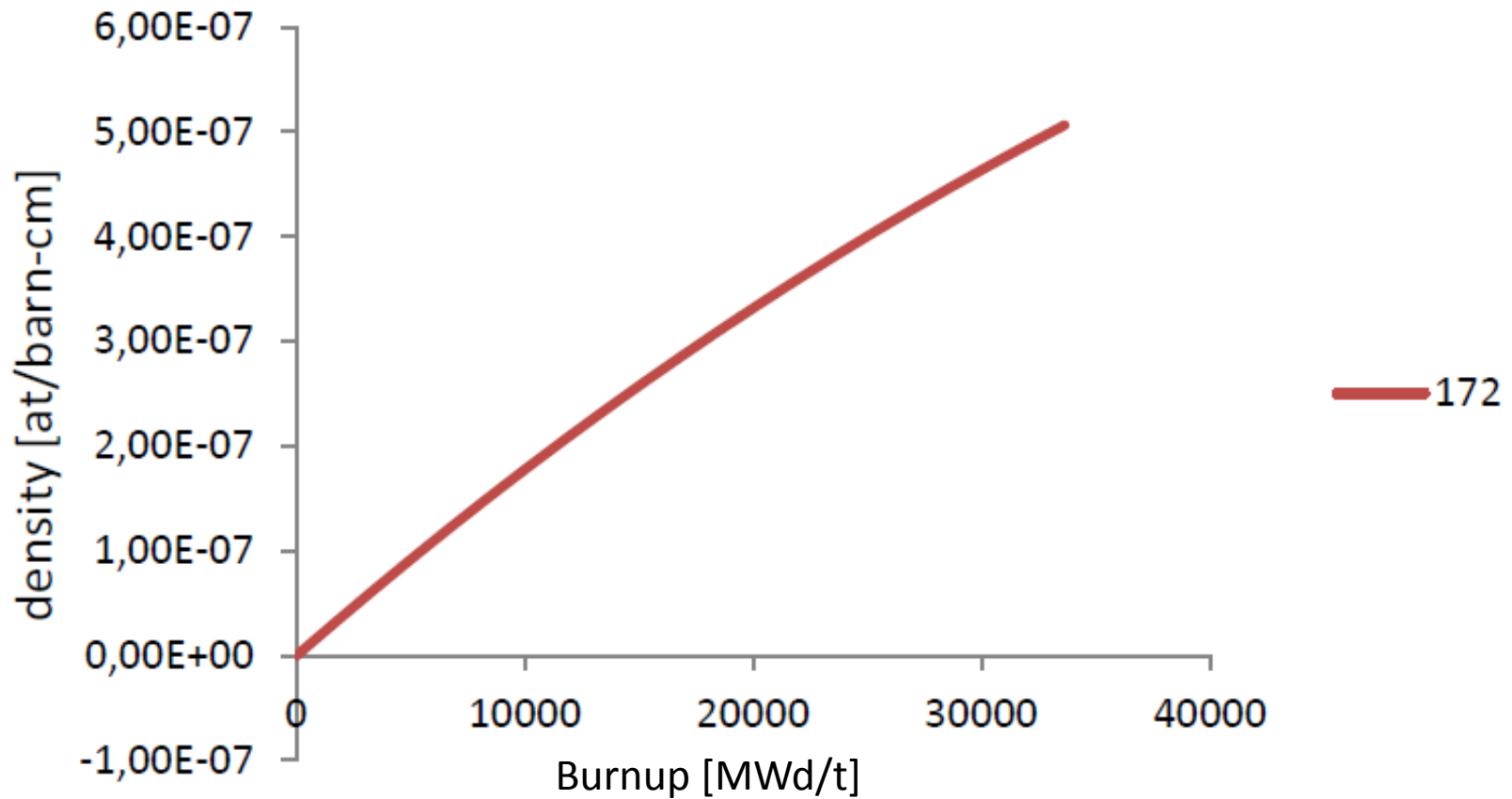


# RESULTS



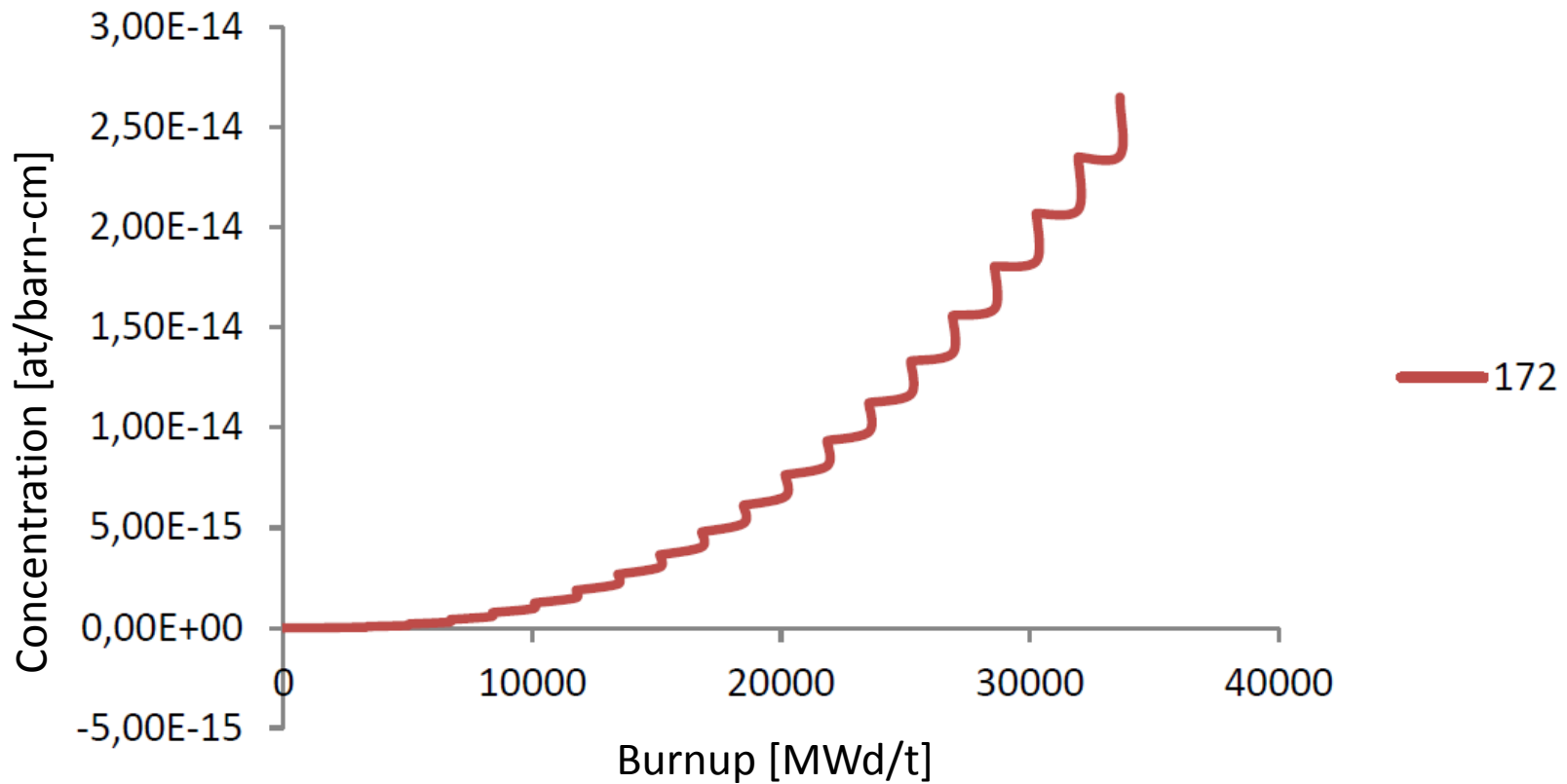
# RESULTS

## Li-6

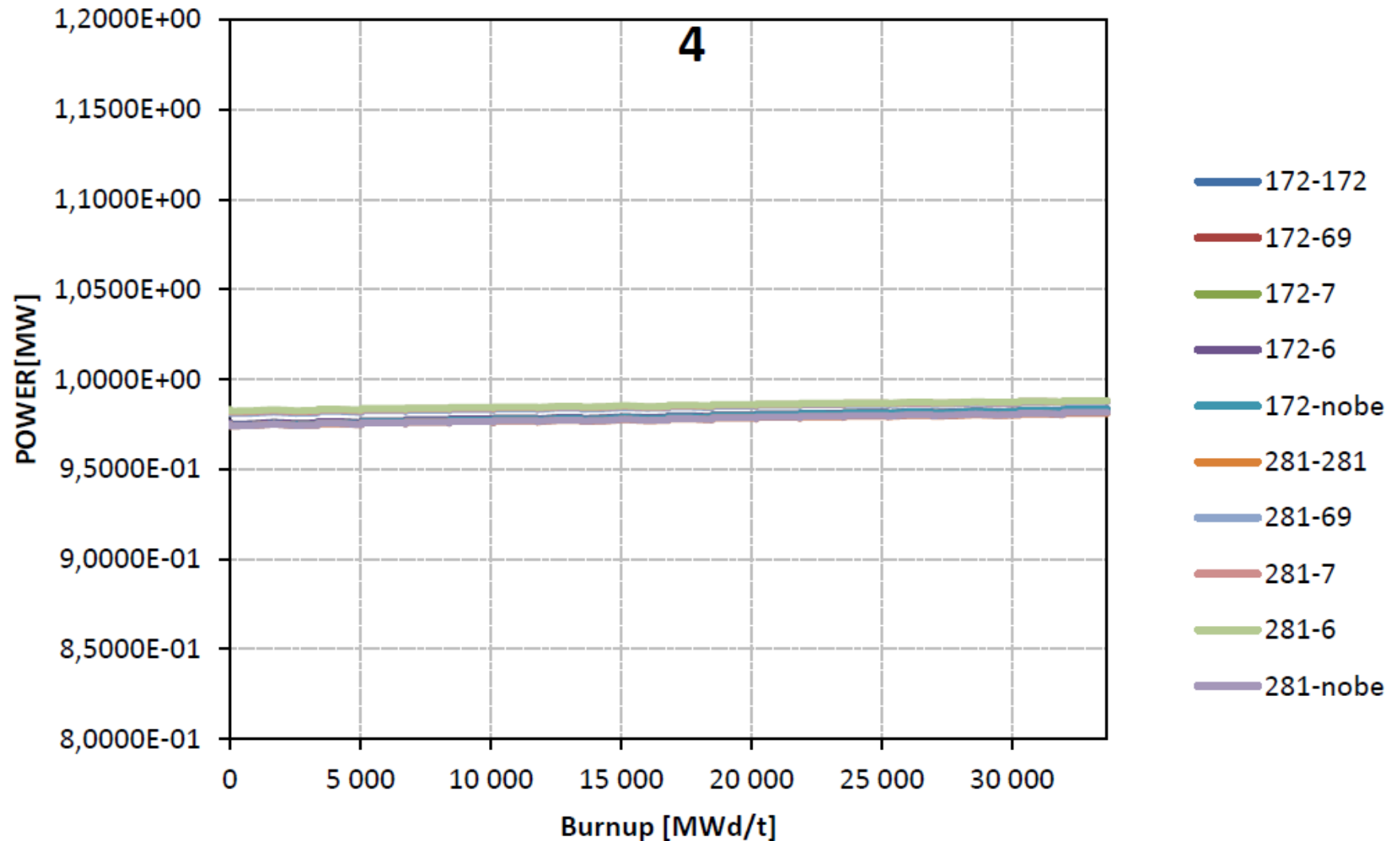


# RESULTS

## He-3



# RESULTS



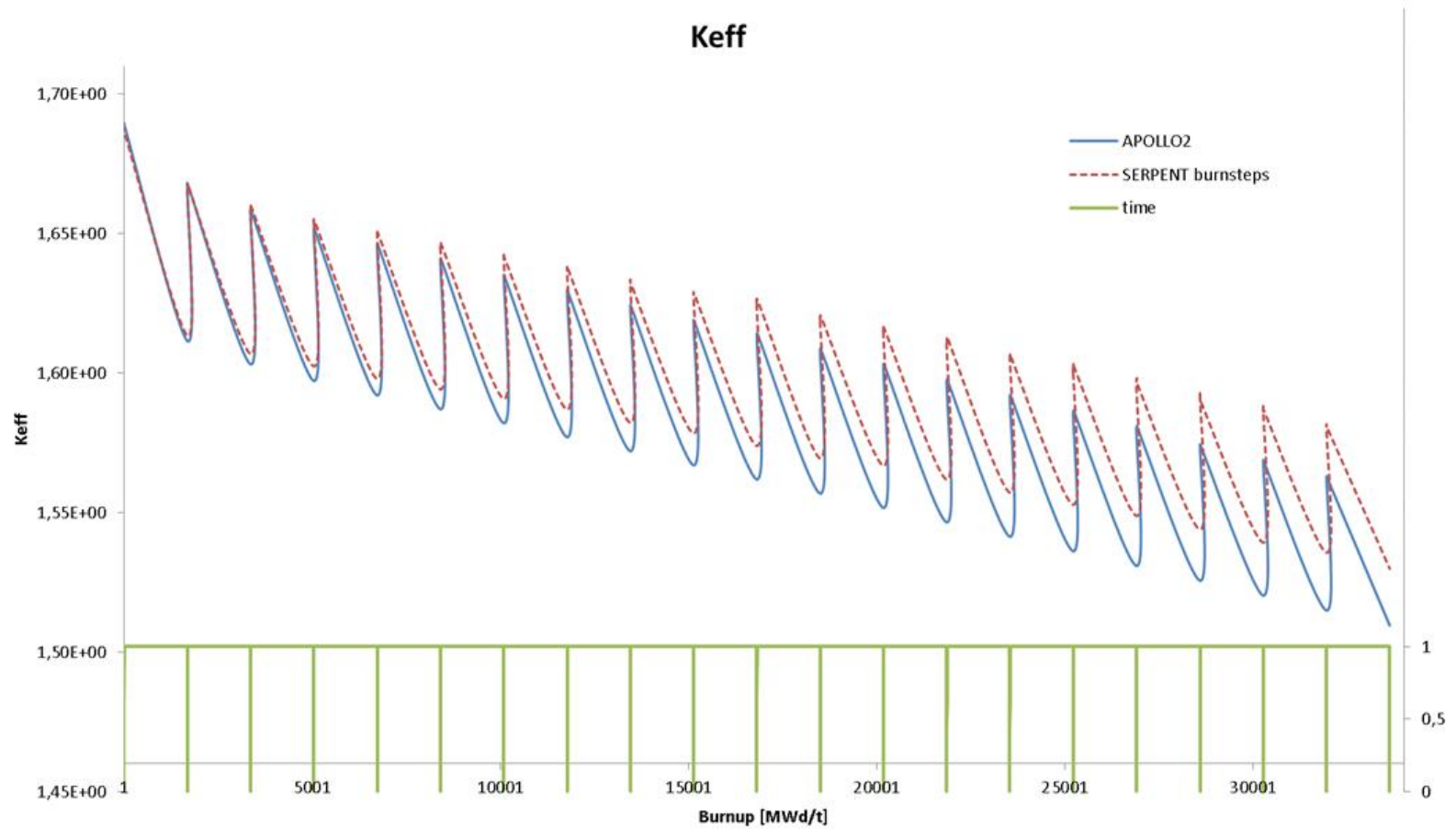
# RESULTS

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Cold conditions

|                 | <b>Keff</b> | <b><math>\Delta</math>keff [pcm]</b> |
|-----------------|-------------|--------------------------------------|
| <b>APOLLO2</b>  | 1.69860     |                                      |
| <b>TRIPOLI4</b> | 1.70989     | 389                                  |
| <b>SERPENT</b>  | 1.69498     | -126                                 |
| <b>MCNP</b>     | 1.70148     | 101                                  |

# RESULTS





# SUMMARY

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- Good agreement for both APOLLO2 methods
- TRIPOLI4 results are acceptable but with relatively high discrepancy
- TRIPOLI4 is not designed to calculate burnup
- SERPENT calculations are promising but need improvement

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THANK YOU!

