
Forward and Inverse Uncertainty Quantification of Thermal-Hydraulics Physical Model Parameters

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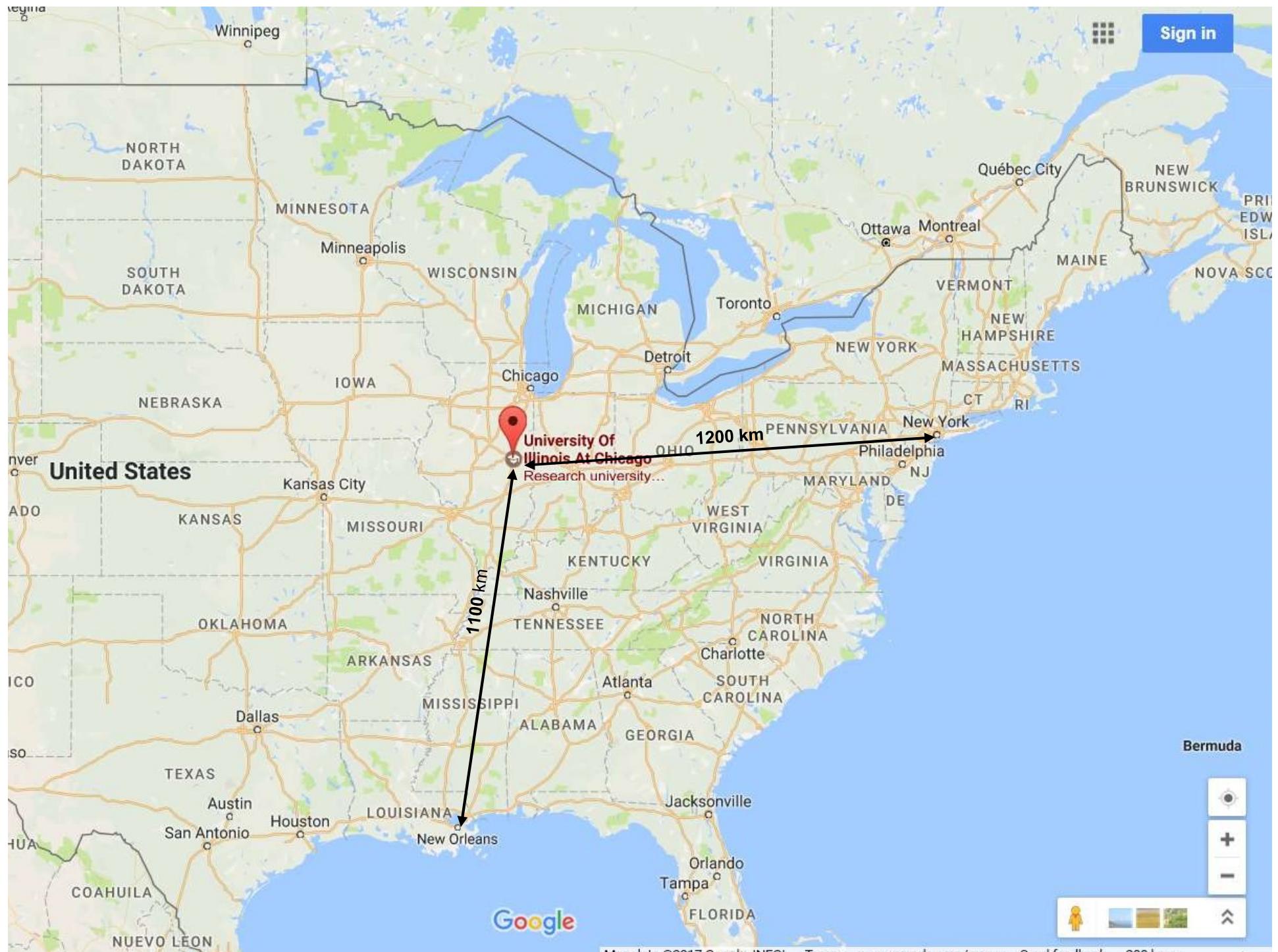
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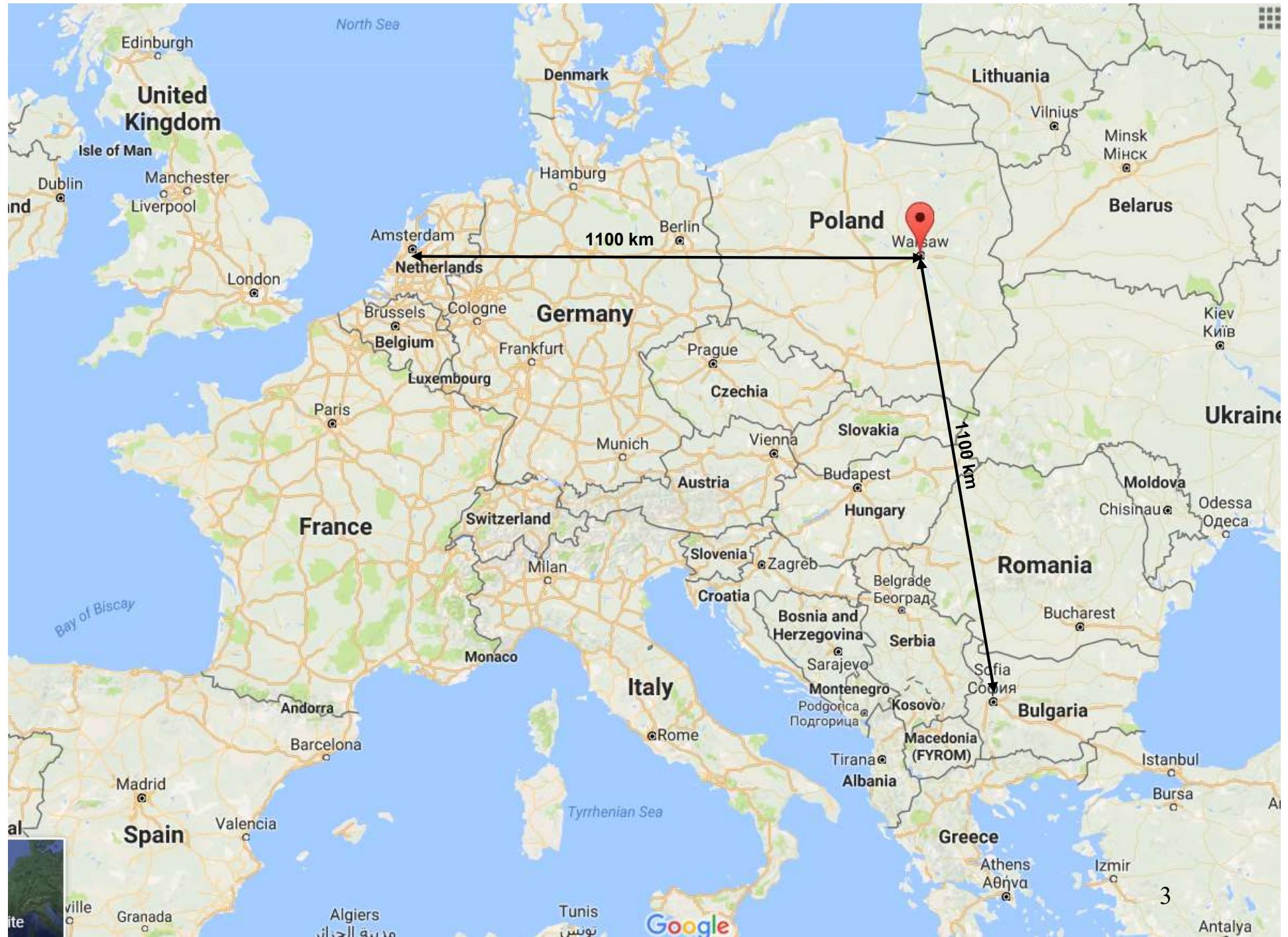
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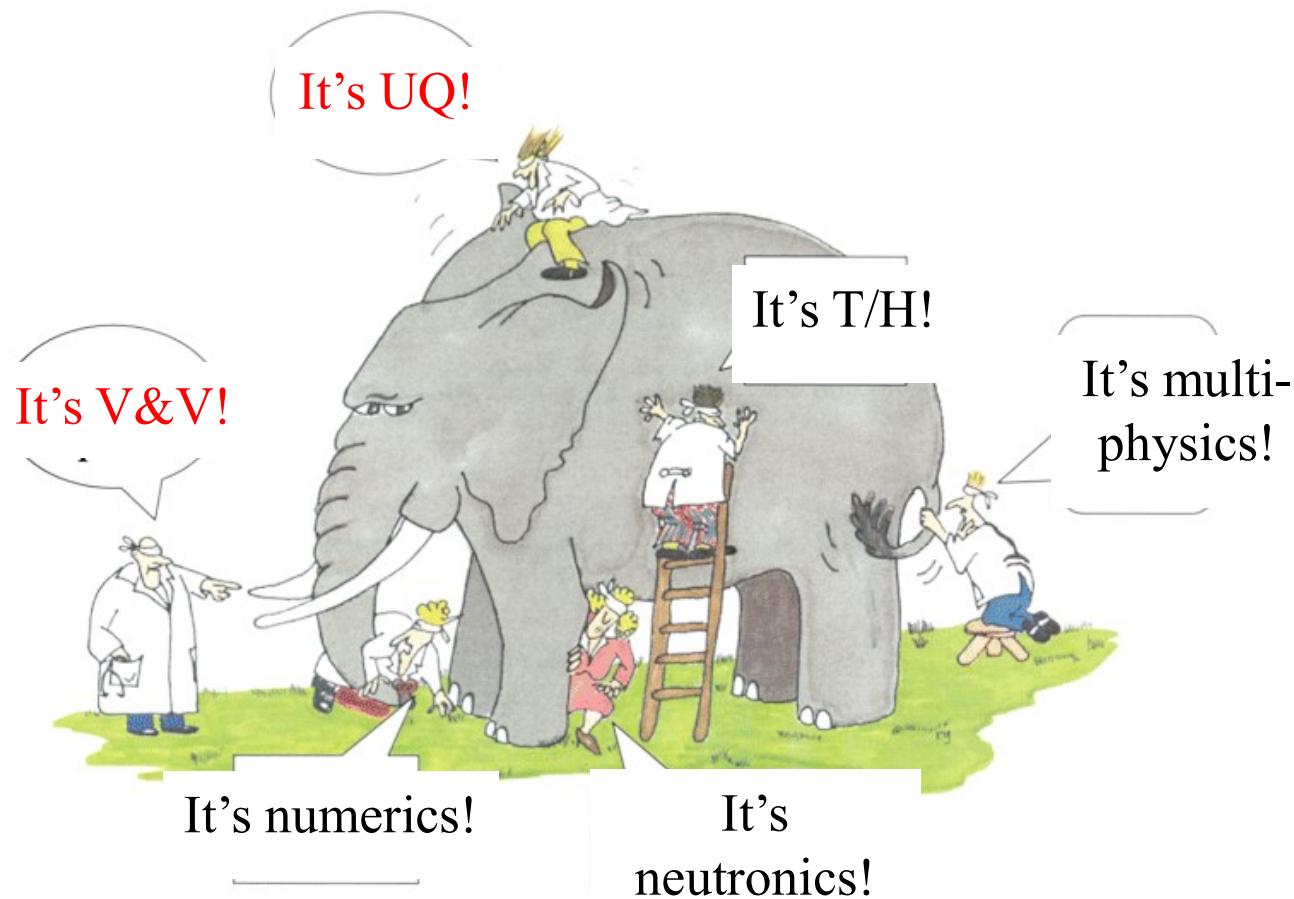
June 20, 2017

Sign in



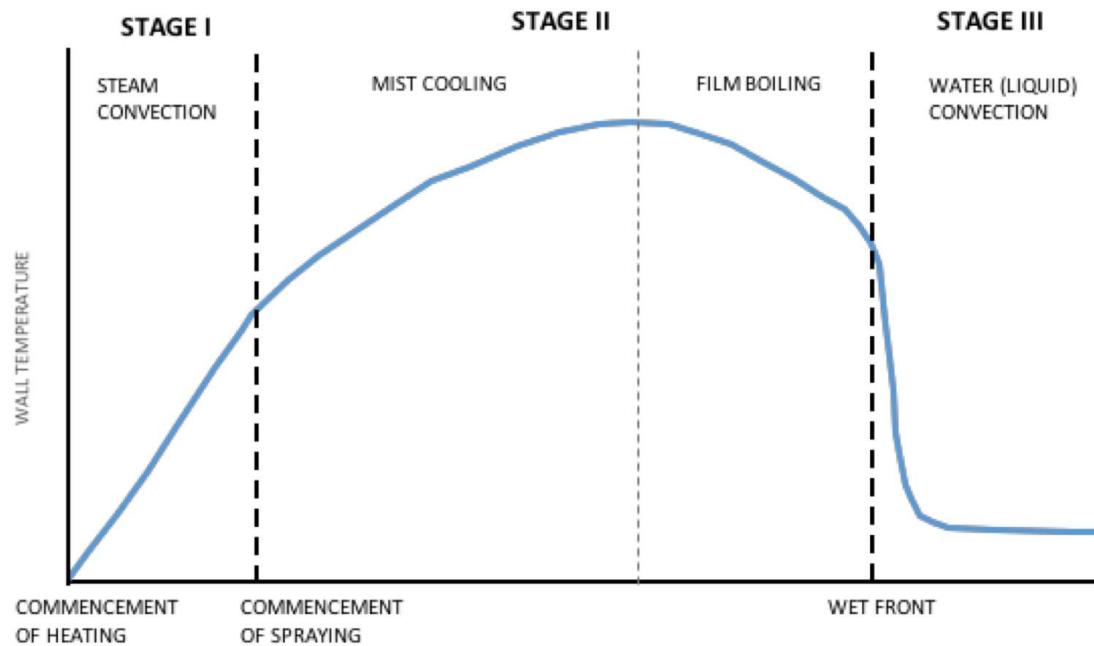


Typical scientific discussion...

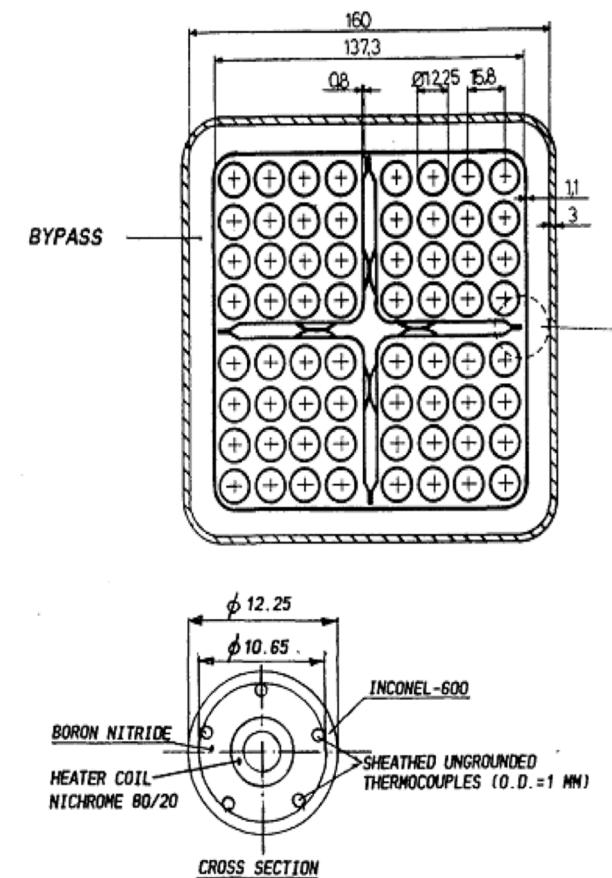
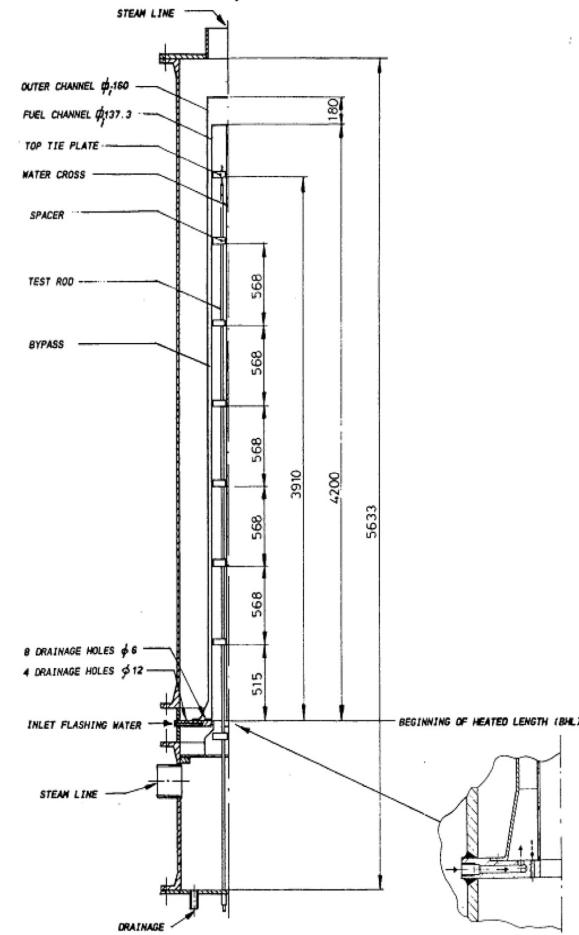
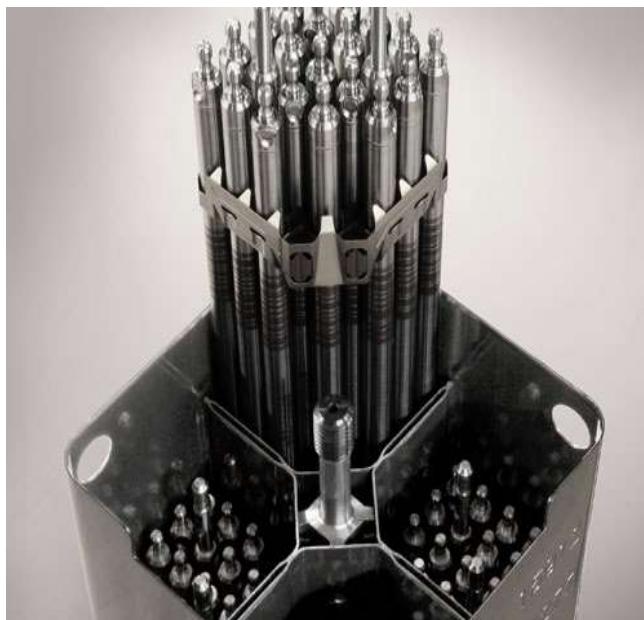


Post-LOCA BWR Spray Cooling

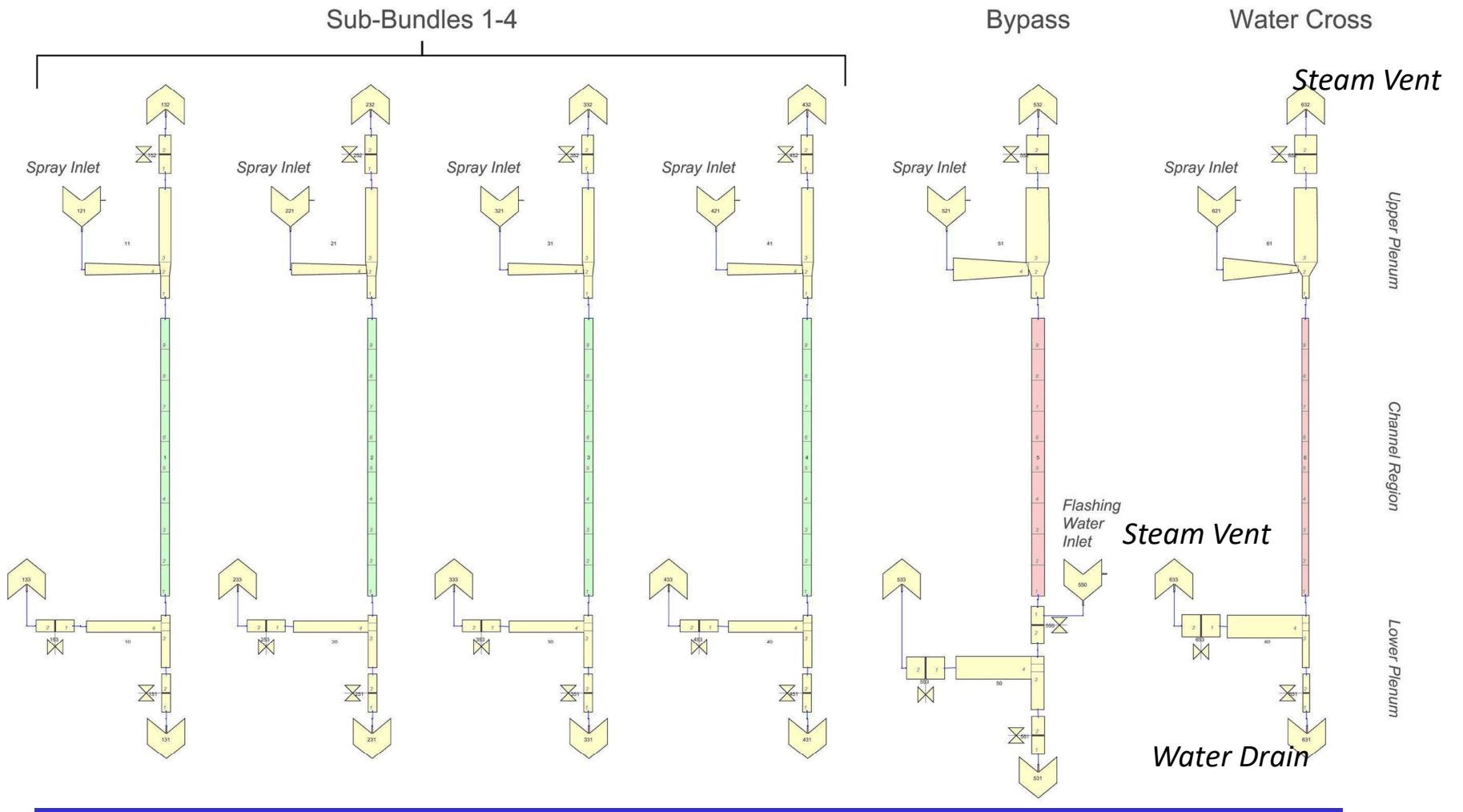
- ◆ Stage I – steam convection (end of blowdown)
- ◆ Stage II – DFFB and post-CHF flow cooling (refill-reflood)
- ◆ Stage III – water film quench, annular flow (reflood)



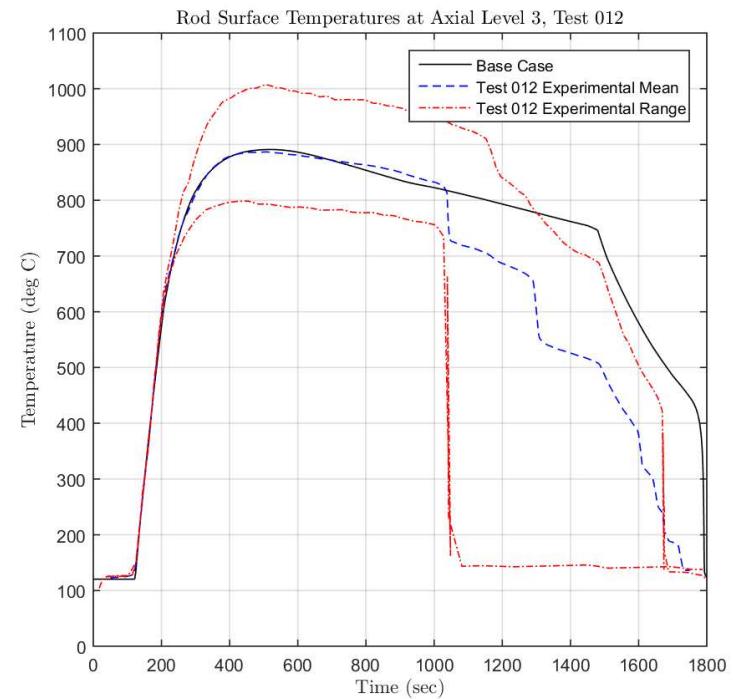
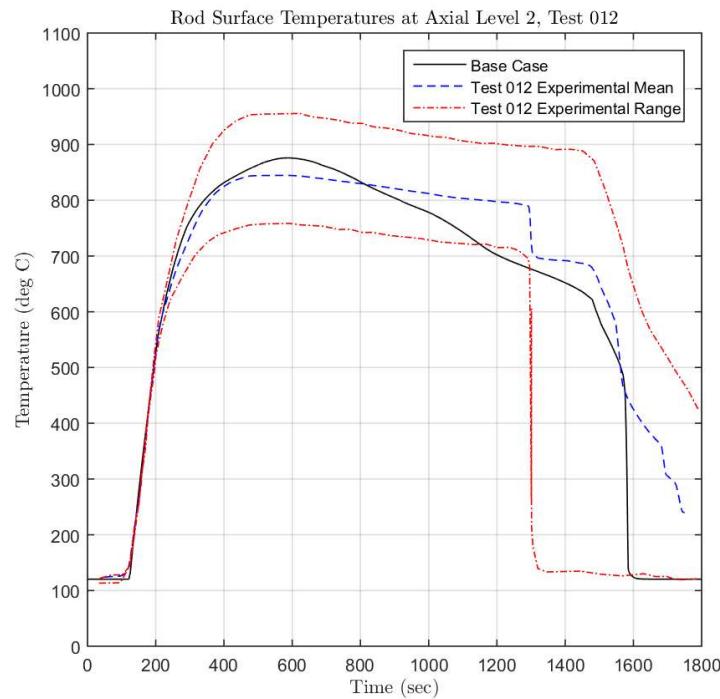
SVEA Spray Cooling Experiment



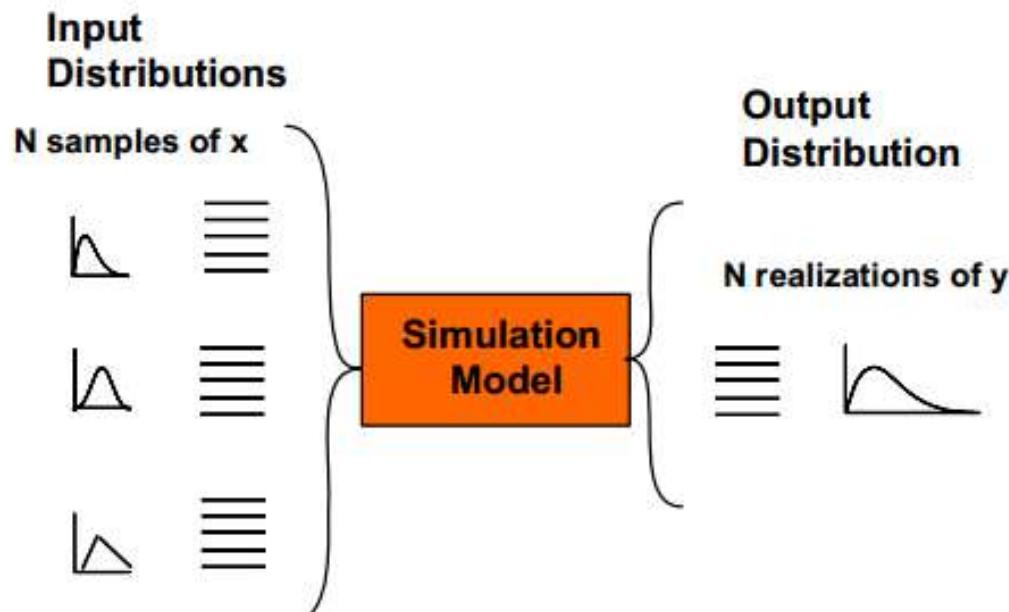
TRACE Model



Test 012 – Uniform spray (40 g/s)



Forward Uncertainty Quantification



Uncertainty Parameters, 1/4

| No. | Parameter | Uncertainty | Reference Value |
|---|-----------------------------|-------------|-----------------|
| Thermal-Hydraulics Initial and Boundary Conditions | | | |
| 1 | Spray system pressure | 0.1 bar | 2 bar |
| 2 | Spray system temperature | 0.75% | 323 K |
| 3 | Bundle spray mass flow | 1% | 20-80 g/s |
| 4 | Bypass spray mass flow | 1% | 65-130 g/s |
| 5 | Water cross spray mass flow | 1% | 10 g/s |
| 6 | Water drain temperature | 0.75% | 323 K |
| 7 | Steam vent temperature | 0.75% | 393 K |
| 8 | Outlet pressure | 0.1 bar | 2 bar |

Uncertainty Parameters, 2/4

| No. | Parameter | Uncertainty | Reference Value |
|----------------------------------|-------------------------------|-------------|----------------------|
| Vessel-related Parameters | | | |
| 9 | Bundle wall roughness | 30% | 1×10^{-6} m |
| 10 | Bypass channel wall roughness | 30% | 1×10^{-6} m |
| 11 | Water-cross wall roughness | 30% | 1×10^{-6} m |
| 12 | Length of main channel | 0.01 m | 3.68 m |
| 13 | Length of bypass channel | 0.01 m | 3.68 m |
| 14 | Length of water-cross | 0.01 m | 3.68 m |

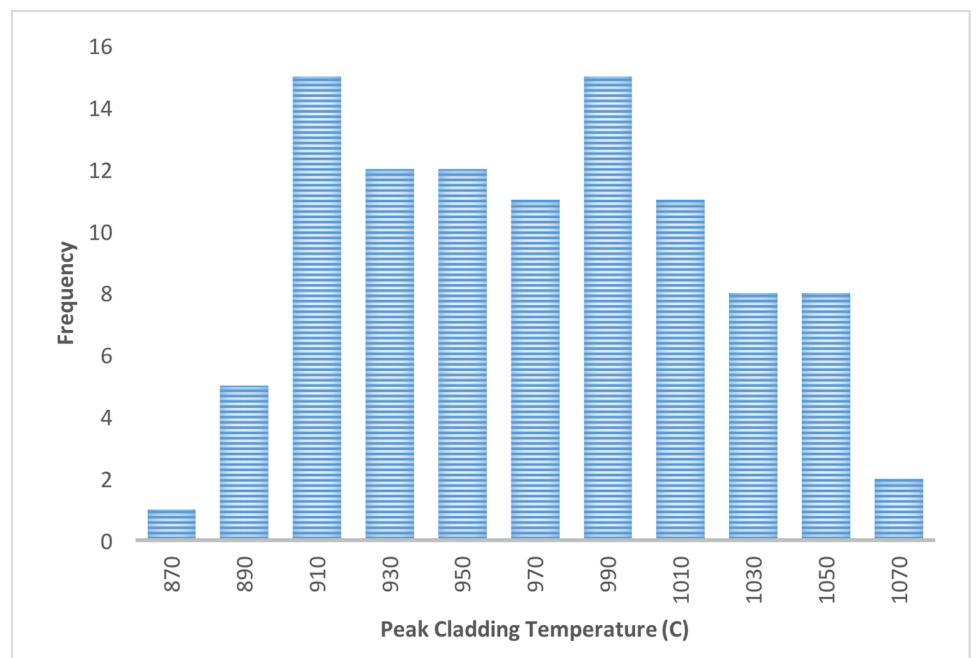
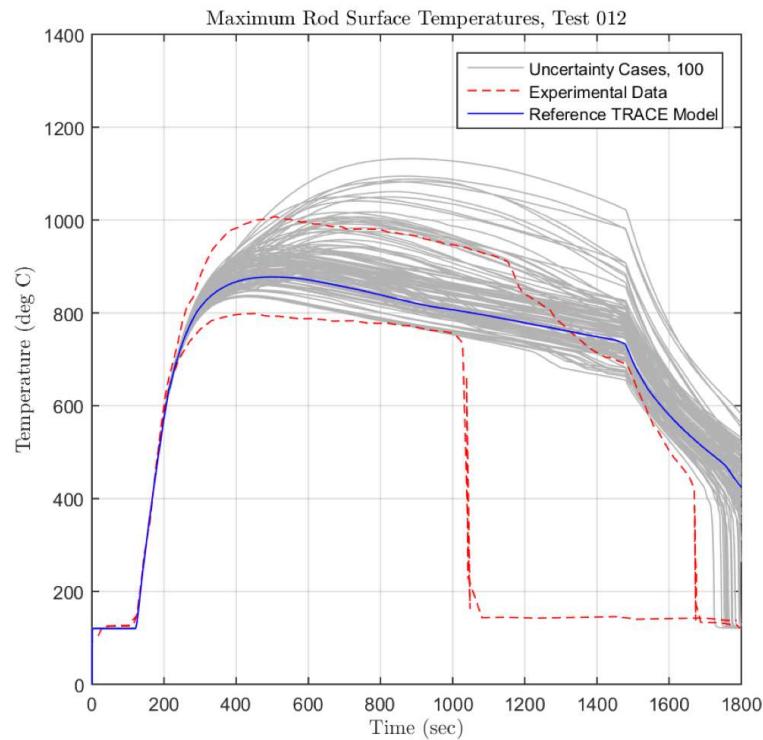
Uncertainty Parameters, 3/4

| No. | Parameter | Uncertainty | Reference Value |
|----------------------------------|--------------------------------|-------------|------------------------------------|
| Bundle-related Parameters | | | |
| 15 | Bundle flow area | 1.00% | $2.428 \times 10^{-3} \text{ m}^2$ |
| 16 | Bundle hydraulic diameter | 1.00% | 0.01114 m |
| 17 | Bypass channel flow area | 1.00% | $6.14 \times 10^{-3} \text{ m}^2$ |
| 18 | Bypass hydraulic diameter | 1.00% | 0.0884 m |
| 19 | Water Cross flow area | 1.00% | $1.612 \times 10^{-3} \text{ m}^2$ |
| 20 | Water Cross hydraulic diameter | 1.00% | 0.0453 m |
| 21 | Rod emissivity | 0.10 | 0.45 |
| 22 | Bundle wall emissivity | 0.10 | 0.3 |
| 23 | CCFL slope | 0.8-1.0 | 1.0 |
| 24 | CCFL constant | 0.88-1.0 | 1.0 |

Uncertainty Parameters, 4/4

| No. | Parameter | Uncertainty | Reference Value |
|--|-------------------------------|-------------|-----------------|
| TRACE Physical Models – Heat Transfer | | | |
| 25 | DFFB Wall-Liquid HTC | 45% | 1.0 |
| 26 | Wall Liquid HTC | 15% | 1.0 |
| 27 | Wall Vapor HTC | 20% | 1.0 |
| 28 | DNB/CHF | 8% | 1.0 |
| TRACE Physical Models – Friction | | | |
| 29 | Annular-Mist Interfacial Drag | 25% | 1.0 |
| 30 | DFFB Interfacial Drag | 40% | 1.0 |
| 31 | Wall Drag | 5% | 1.0 |

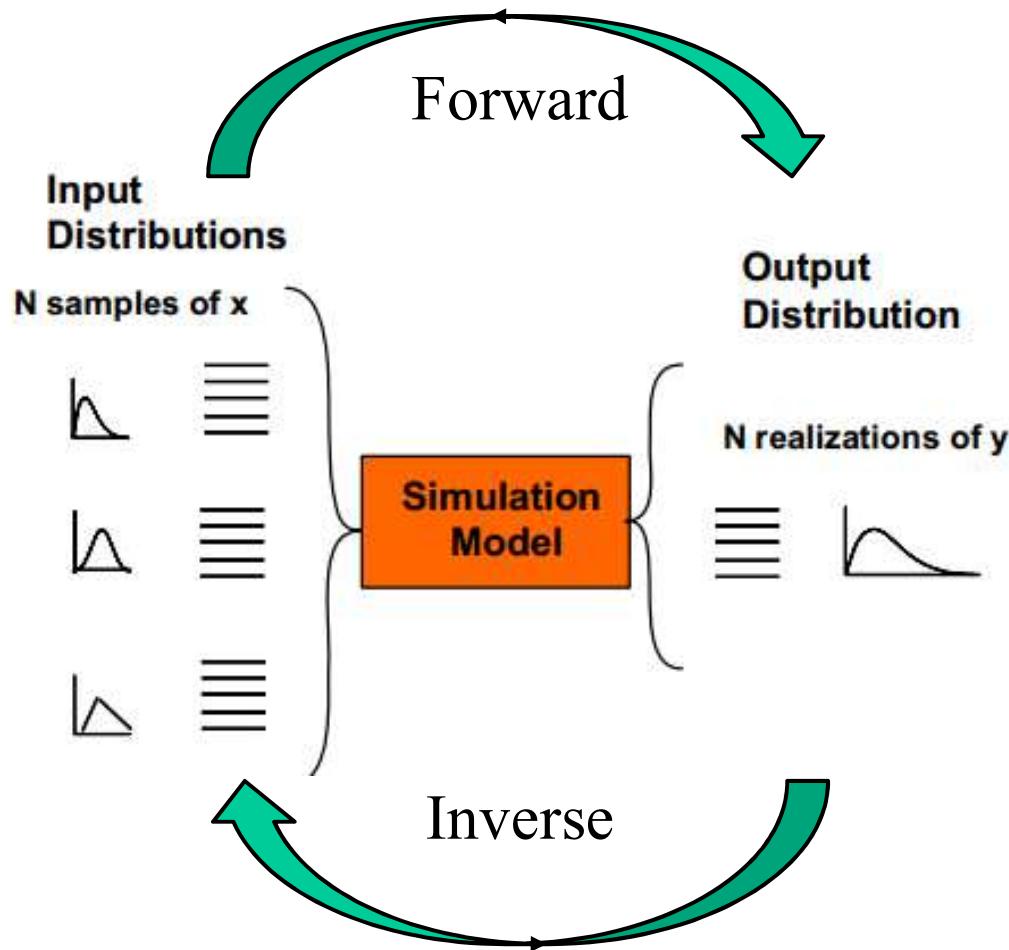
DAKOTA simulation – 100 cases



Uncertainty of Physical Models

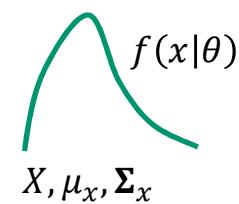
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Forward vs Inverse Uncertainty Quantification

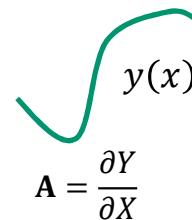


Forward vs Inverse Uncertainty Quantification

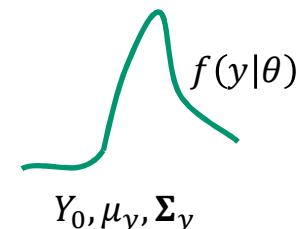
Forward



INPUT



CODE



OUTPUT

Physical models
Geometry
IC and BCs

TRACE/RELAP
BISON...

Temperature
Pressure drop
Void fraction...

Inverse



Notations & Definitions

Meaning of variables

| Variables | Meaning |
|-------------------------|---|
| \vec{X} | input model parameter random variable |
| \vec{Y} | output random variable from experimental measurement |
| \vec{Y}_0 | output random variable from code prediction |
| \vec{E} | random error of experimental measurement |
| \mathbf{A} | sensitivity coefficient matrix |
| $\vec{\mu}_x, \Sigma_x$ | mean and covariance matrix of input model parameter random variable |
| $\vec{\mu}_y, \Sigma_y$ | mean and covariance matrix of output random variable |
| $\vec{\mu}_e, \Sigma_e$ | mean and covariance matrix of random error of experimental measurement |
| $\vec{\theta}$ | parameter vector of the mean and variance of input model parameter |

Notations & Definitions

- ◆ Likelihood $L(\vec{\theta}|x)$: The probability that observed x happens with parameter $\vec{\theta}$.

$$L(\vec{\theta}|x) \equiv f(x; \vec{\theta})$$

- ◆ Prior $\pi(\vec{\theta})$: Our prior knowledge about the parameters $\vec{\theta}$.
- ◆ Posterior $\pi(\vec{\theta}|x)$: Our updated knowledge about the parameter $\vec{\theta}$ after considering both the observed value x and prior knowledge.

$$\pi(\vec{\theta}|x) = \frac{L(\vec{\theta}|x)\pi(\vec{\theta})}{\int L(\vec{\theta}|x)\pi(\vec{\theta})d\vec{\theta}} \equiv K(x)L(\vec{\theta}|x)\pi(\vec{\theta})$$

Assumptions

- ◆ \vec{X} has a joint Gaussian distribution

$$f(\vec{x}; \vec{\theta}) = \frac{1}{2\pi} |\Sigma_x|^{-\frac{1}{2}} \exp[-\frac{1}{2} (\vec{x} - \vec{\mu}_x)^T \Sigma_x^{-1} (\vec{x} - \vec{\mu}_x)]$$

- ◆ $\delta \vec{Y}$ depends linearly on $\delta \vec{X}$ when $\delta \vec{X}$ is small

$$\vec{Y} = \vec{Y}_0 + \mathbf{A} \vec{X}$$

where, the sensitivity coefficient matrix is obtained by,

$$\mathbf{A} = \frac{\partial \vec{Y}}{\partial \vec{X}}, \quad \text{evaluated at nominal X}$$

\vec{Y} also follows joint Gaussian distribution, because of the linear relation.

- ◆ \vec{E} is assumed to be mean-zero

$$\vec{Y} = \vec{Y}_0 + \mathbf{A} \vec{X} + \vec{E}$$

Likelihood function & Posterior distribution

Suppose there are $i = 1, 2, \dots, N$ sets of observed data (or experiments), we assume \vec{Y}_i 's are independent to each other. Then we have,

$$\vec{Y}_i = \vec{Y}_{0,i} + \mathbf{A}_i \vec{X} + \vec{E}_i$$

$$f_i(\vec{y}; \vec{\theta}) = \frac{1}{2\pi} |\Sigma_{y,i}|^{-\frac{d_y}{2}} \exp[-\frac{1}{2} (\vec{y} - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y} - \vec{\mu}_{y,i})]$$

with,

$$\vec{\mu}_{y,i} = \vec{Y}_{0,i} + \mathbf{A}_i \vec{\mu}_x$$

$$\Sigma_{y,i} = \mathbf{A}_i \Sigma_x \mathbf{A}_i^T + \Sigma_{e,i}$$

The likelihood function $L(\vec{\theta} | \mathbf{y})$ and posterior distribution $\pi(\vec{\theta} | \mathbf{y})$ is,

$$L(\vec{\theta} | \mathbf{y}) = \prod_{i=1}^N \frac{1}{2\pi} |\Sigma_{y,i}|^{-\frac{d_y}{2}} \exp[-\frac{1}{2} (\vec{y}_i - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i})]$$

$$\pi(\vec{\theta} | \mathbf{y}) = K(\mathbf{y}) \pi(\vec{\theta}) \prod_{i=1}^N \frac{1}{2\pi} |\Sigma_{y,i}|^{-\frac{d_y}{2}} \exp[-\frac{1}{2} (\vec{y}_i - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i})]$$

Notes: The likelihood function and posterior distribution are the base for following MLE, MAP and MCMC algorithm.

MLE

Idea: maximize the likelihood function to solve for parameter vector $\vec{\theta}$

E-M algorithm:

- ◆ Maximization. With Σ_x known, $\vec{u}_{x,\text{new}}$ is solved by maximizing the Log-likelihood function.

$$\vec{u}_{x,\text{new}} = \max_{\vec{u}_x} \text{log}L(\vec{\theta}|\mathbf{y})$$

with the Log-likelihood function,

$$\text{log}L(\vec{\theta}|\mathbf{y}) = \sum_{i=1}^N \left[-\frac{d_y}{2} \log |\Sigma_{y,i}| - \log 2\pi - \frac{1}{2} (\vec{y}_i - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i}) \right]$$

- ◆ Expectation. With $\vec{u}_{x,\text{new}}$ known, Σ_x is updated using conditional expectation.

$$\Sigma_{x,\text{new}} = E[(\vec{X} - \vec{u}_{x,\text{new}})(\vec{X} - \vec{u}_{x,\text{new}})^T | \mathbf{y}]$$

MLE: E-M algorithm

- ◆ Maximization step (update mean value)

Let the derivative of the log-likelihood function with respect to $\vec{\mu}_x$ to be zero,

$$\frac{\partial \log L(\vec{\theta} | \mathbf{y})}{\partial \vec{\mu}_x} = \frac{\partial \sum_{i=1}^N \left[-\frac{d_y}{2} \log |\Sigma_{y,i}| - \log 2\pi - \frac{1}{2} (\vec{y}_i - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i}) \right]}{\partial \vec{\mu}_x} = 0$$

We get the equation to update mean value,

$$\left(\sum_{i=1}^N \mathbf{A}_i^T \Sigma_{y,i}^{-1} \mathbf{A}_i \right) \vec{\mu}_{x,\text{new}} = \sum_{i=1}^N \mathbf{A}_i^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{y}_{0,i})$$

- ◆ Expectation step (update covariance)

After the mean value $\vec{\mu}_x$ has been updated, the covariance matrix is updated by:

$$\begin{aligned} \Sigma_{x,\text{new}} &= E[(\vec{X} - \vec{\mu}_{x,\text{new}})(\vec{X} - \vec{\mu}_{x,\text{new}})^T | \mathbf{y}] \\ &= \Sigma_{x,\text{old}} + \frac{1}{N} \sum_{i=1}^N (-\Sigma_{xy,i}^T \Sigma_{y,i}^{-1} \Sigma_{xy,i} + [\Sigma_{xy,i}^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i})][\Sigma_{xy,i}^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i})]^T) \end{aligned}$$

where $\Sigma_{xy,i}$ is correlation matrix,

$$\Sigma_{xy,i} = \text{cov}(\vec{X}, \vec{Y}_i) = \mathbf{A}_i \Sigma_x$$

MAP

Idea: maximize the posterior distribution to solve for the parameter vector $\vec{\theta}$

Difference with MLE: prior distribution $\pi(\vec{\theta})$ and constant $K(\mathbf{y})$

$$\pi(\vec{\theta}|\mathbf{y}) = K(\mathbf{y})\pi(\vec{\theta}) \prod_{i=1}^N \frac{1}{2\pi} |\Sigma_{y,i}|^{-\frac{d_y}{2}} \exp[-\frac{1}{2}(\vec{y}_i - \vec{\mu}_{y,i})^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{\mu}_{y,i})]$$

- ◆ Maximization step needs considering prior distribution effect,

$$(\sum_{i=1}^N \mathbf{A}_i^T \Sigma_{y,i}^{-1} \mathbf{A}_i + \mathbf{M}_{\pi}) \vec{\mu}_{x,\text{new}} = \sum_{i=1}^N \mathbf{A}_i^T \Sigma_{y,i}^{-1} (\vec{y}_i - \vec{y}_{0,i}) + \vec{B}_{\pi}$$

\mathbf{M}_{π} and \vec{B}_{π} depends on the prior distribution in practical application.

- ◆ Expectation step is the same as MLE.

$$\text{Recall: } \pi(\vec{\theta}|x) = \frac{L(\vec{\theta}|x)\pi(\vec{\theta})}{\int L(\vec{\theta}|x)\pi(\vec{\theta})d\vec{\theta}} \equiv K(x)L(\vec{\theta}|x)\pi(\vec{\theta})$$

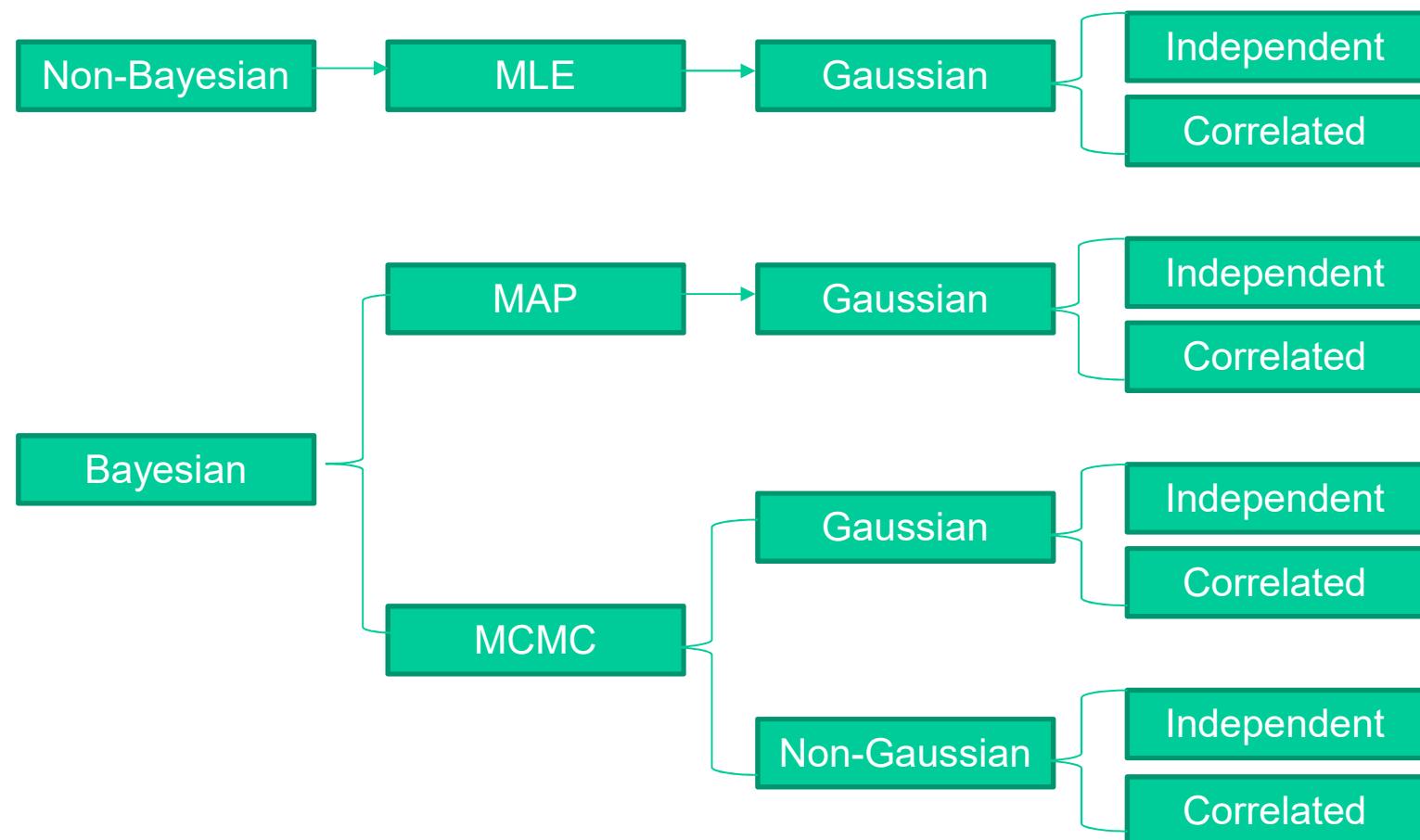
MCMC

Problems with MLE and MAP

- ◆ $L(\vec{\theta}|\mathbf{y})$. Maximization of likelihood function is difficult for distribution other than Gaussian distribution.
- ◆ $\pi(\vec{\theta})$. Should be differentiable to be used in MAP algorithm.
- ◆ $K(\mathbf{y})$. Has to be obtained with a multi-dimensional integration.

MCMC: sample the posterior distribution without performing the integration for $K(\mathbf{y})$. This sampling is implemented by using an iterative Monte Carlo sampling, which usually forms a Markov Chain.

Inverse Methods for Parameter Estimation

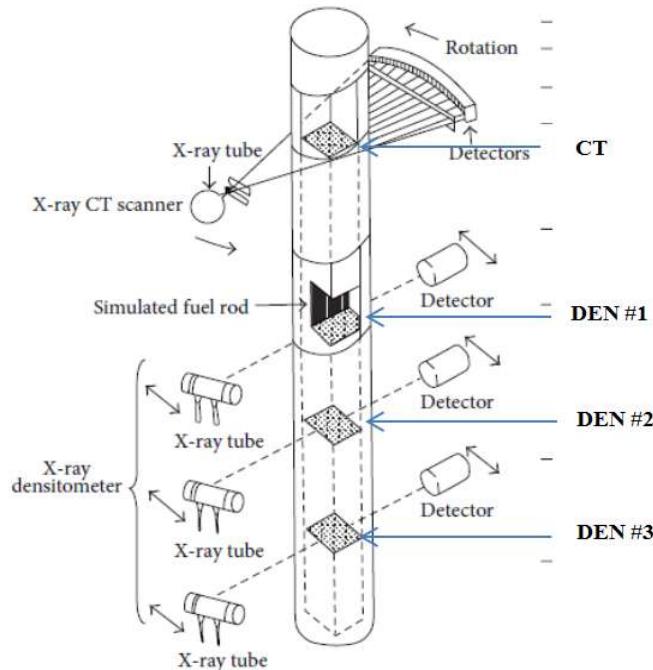


Distinguished by statistical methods

Distinguished by distribution of \vec{X}

Application: BFBT introduction

BFBT benchmark: The BFBT benchmark is a valuable benchmark for the sub-channel analysis of two-phase flow in BWR rod bundles.



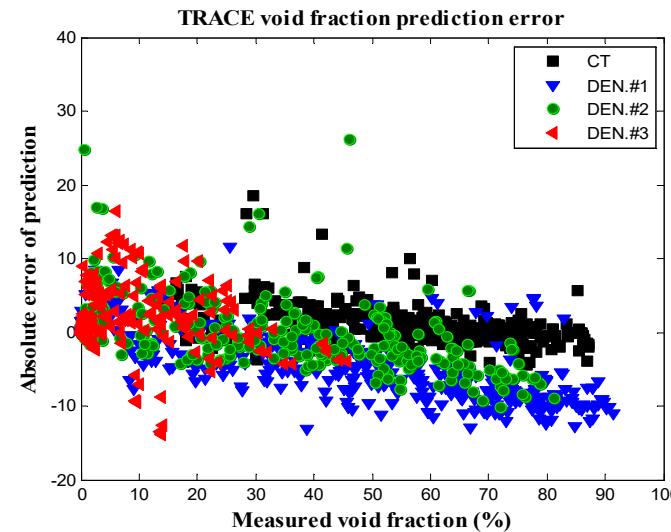
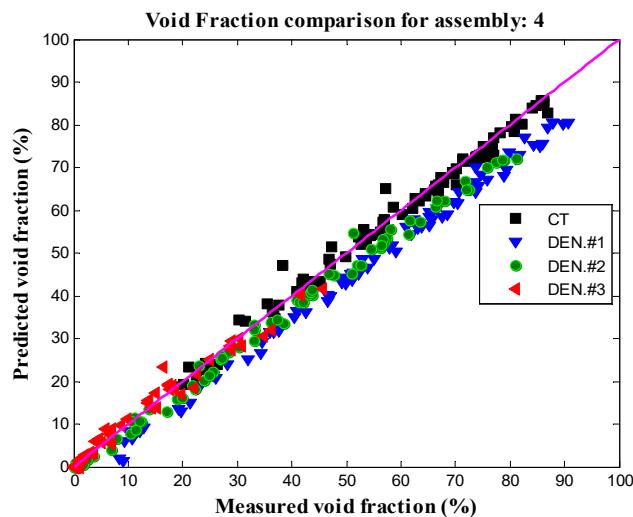
| Parameters | Variations |
|--------------------------|------------|
| Pressure (MPa) | 3.9 - 8.7 |
| Inlet temperature (°C) | 238 - 292 |
| Inlet subcooling (kJ/kg) | 50. - 56. |
| Flow rate (t/h) | 10. - 70. |
| Power (MW) | 0.62 - 7.3 |
| Exit quality (%) | 8 - 25 |
| Exit void fraction (%) | 45 - 90 |

Application: analysis steps

1. Accuracy analysis: compare TRACE predictions with measurements. ($\vec{Y}_0, \vec{Y}, \vec{E}$)
 2. Sensitivity analysis: obtain sensitivity coefficient matrix using TRACE. (\mathbf{A})
 3. Linearity assumption validation. (\mathbf{A})
 4. Inverse uncertainty quantification: estimate with MLE, MAP and MCMC. ($\vec{\mu}_x, \Sigma_x$)
 5. Validate MLE, MAP and MCMC results. ($\vec{\mu}_x, \Sigma_x$)
-

Step 1: Accuracy analysis of TRACE prediction

TRACE void fraction predictions: at 4 axial elevations, and compared with the experimental measurement data.



Step 2: Sensitivity analysis of model parameters

Sensitivity coefficient: approximated with TRACE using finite difference method

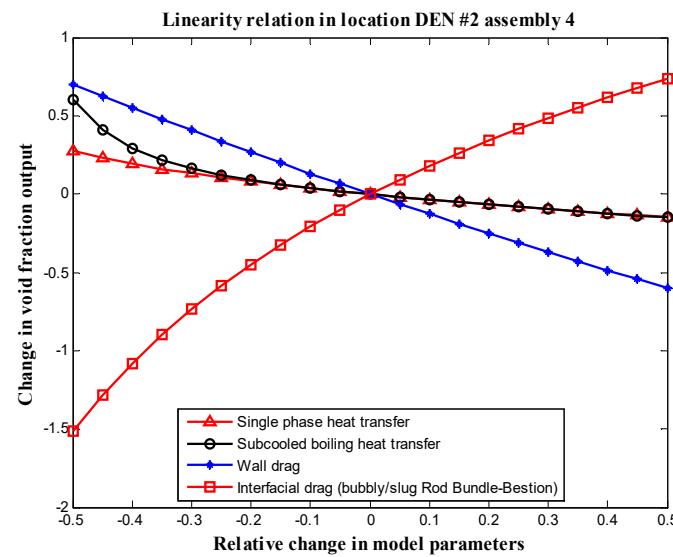
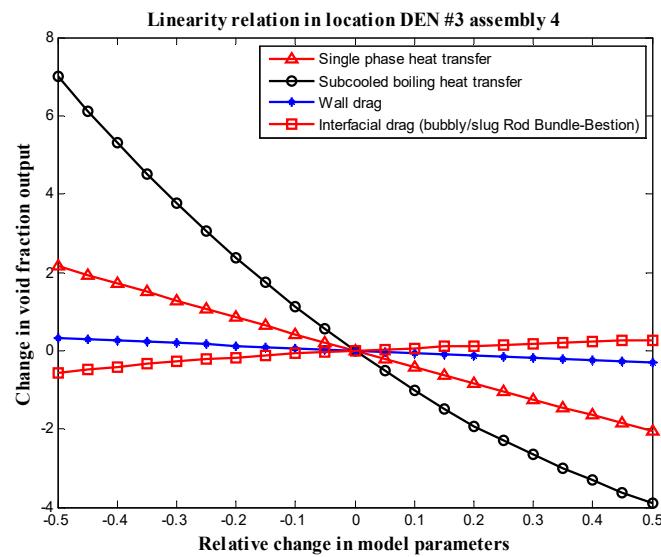
| Parameters | DEN #3 | DEN #2 | DEN #1 | CT |
|---|--------|--------|--------|-------|
| Single phase liquid to wall heat transfer | -4.22 | -0.36 | -0.20 | -0.03 |
| Subcooled boiling heat transfer | -10.77 | -0.38 | -0.20 | -0.03 |
| Wall drag | -0.63 | -1.28 | -1.66 | -2.97 |
| Interfacial drag (bubbly/slug rod rundle-Bestion) | 0.73 | 1.94 | 2.25 | 0.93 |

Sensitivity coefficient = $\frac{\Delta Y}{\Delta X} \times 100\%$

Step 3: Linearity assumption validation

Approach: obtain $\vec{Y}(\vec{X})$ using TRACE

Result: linearity assumption is valid in the relative range [-0.5, 0.5]



Step 4: Inverse uncertainty quantification

Criterion for selecting data:

1. The measured void fraction should be positive.
2. The predicted void fraction should be positive.
3. The absolute value of sensitivity coefficient should be larger than a pre-set tolerance (0.1).

Prior distribution:

- Conjugate prior distribution for MAP

| Variables | Meaning | Value |
|-----------------|---|---------------|
| \vec{r} | shape factor of normal-inverse gamma distribution | $(3,3)^T$ |
| \vec{k} | shape factor of normal-inverse gamma distribution | $(1.0,1.0)^T$ |
| $\vec{\beta}$ | expectation value of prior $\vec{\mu}$ | $(1.0,1.0)^T$ |
| $\vec{\lambda}$ | expectation value of prior $\vec{\sigma}^2$ | $(1.0,1.0)^T$ |

- Prior distribution for MCMC

| Algorithms | Prior type | Prior distribution |
|------------|-----------------|--|
| MCMC 1 | Non-informative | $\frac{1}{(\sigma^1)^2(\sigma^2)^2}$ |
| MCMC 2 | Conjugate | previous Table |
| MCMC 3 | Uniform | $\vec{\mu} \in [0.5,1.5] \times [0.5,1.5]$, $\vec{\sigma}^2 \in [0., 1.0] \times [0., 1.0]$ |

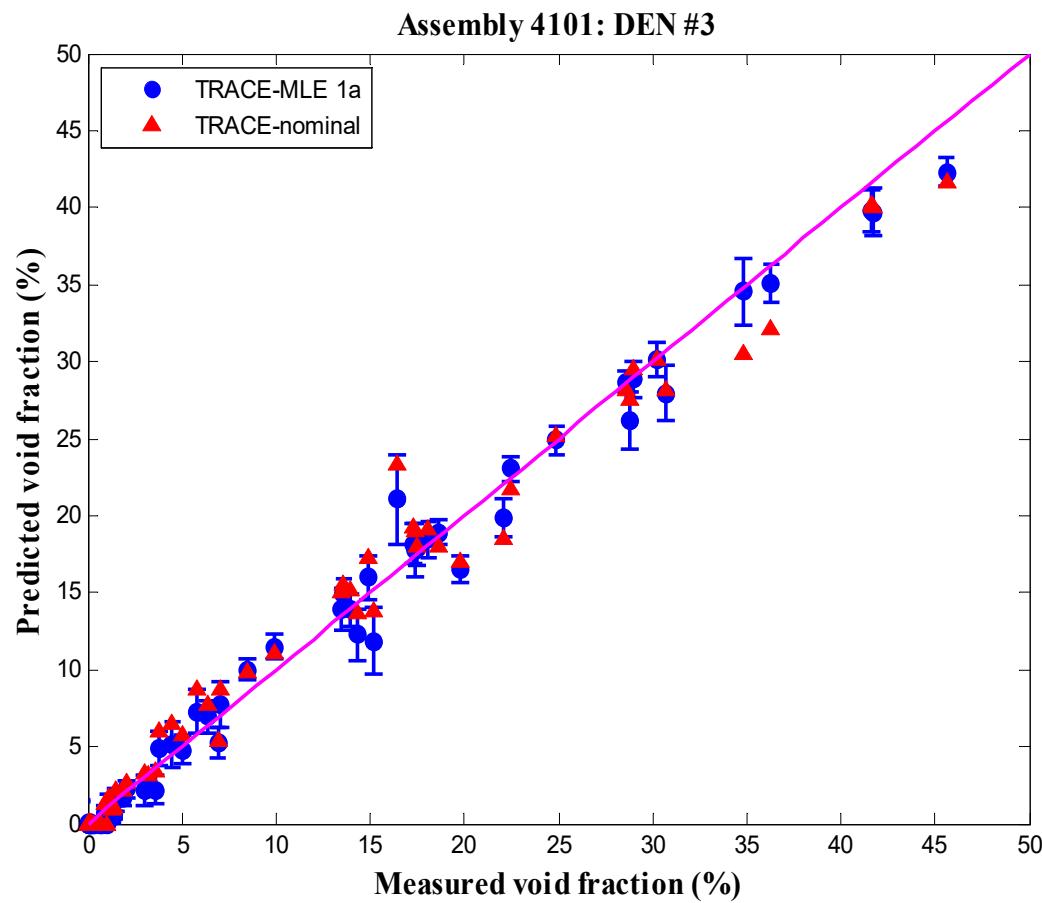
Step 4: IUQ with MLE, MAP, MCMC

Compare results

- ◆ MLE results: information from data
- ◆ MLE vs MCMC 1: very close, because non-informative prior does not provide prior information
- ◆ MLE vs MAP, MCMC 2 and MCMC 3: the results are weighted by prior information.

| Algorithms | Subcooled boiling HTC | Interfacial drag(bubbly/slug) | Correlation |
|------------|-----------------------|-------------------------------|-------------|
| MLE | 1.15 ± 0.05 | 1.70 ± 0.17 | 0.31 |
| MAP | 1.06 ± 0.21 | 1.24 ± 0.46 | 0.16 |
| MCMC 1 | 1.15 ± 0.05 | 1.69 ± 0.21 | N/A |
| MCMC 2 | 1.11 ± 0.29 | 1.46 ± 0.52 | N/A |
| MCMC 3 | 1.11 ± 0.12 | 1.32 ± 0.50 | N/A |

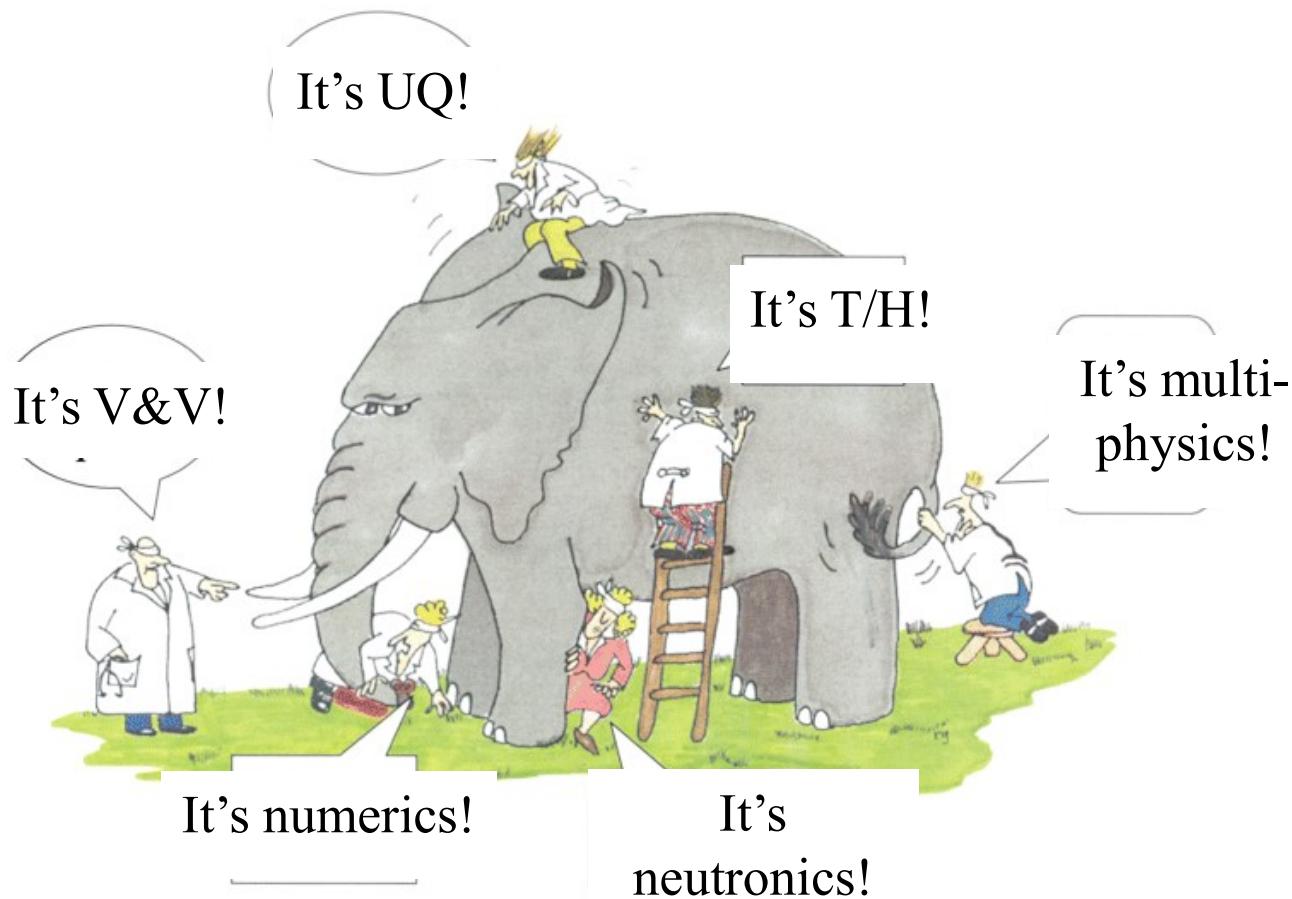
Step 5: Forward uncertainty propagation (validation of inverse uncertainty)



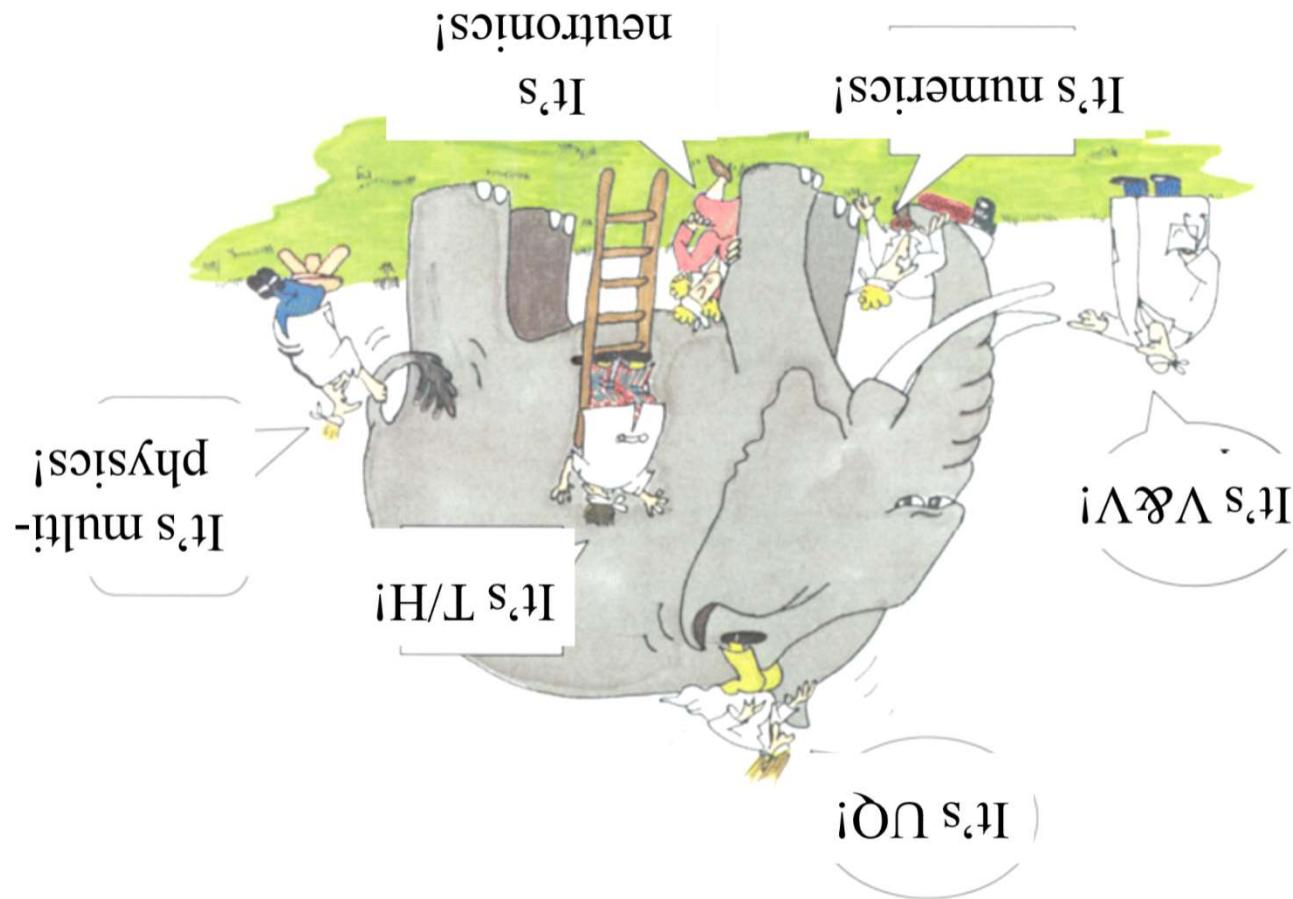
Conclusions

- ◆ Quantification of uncertainties of **input physical models** is possible
 - No need to guess input model uncertainty, no need of expert judgment
 - But methodology cannot be used as black box
- ◆ Facilitates in subsequent forward UQ endeavors
- ◆ Challenges
 - Prior information: we should provide appropriate prior distribution. If not, use MLE instead.
 - Linearity assumption between input and output: use high-order surrogate model
- ◆ Additional application
 - Extendible to other system/codes (**RELAP5, MELCOR, BISON, ...**)
 - Extendible to other fields: **insurance, finance, operations research, ...**

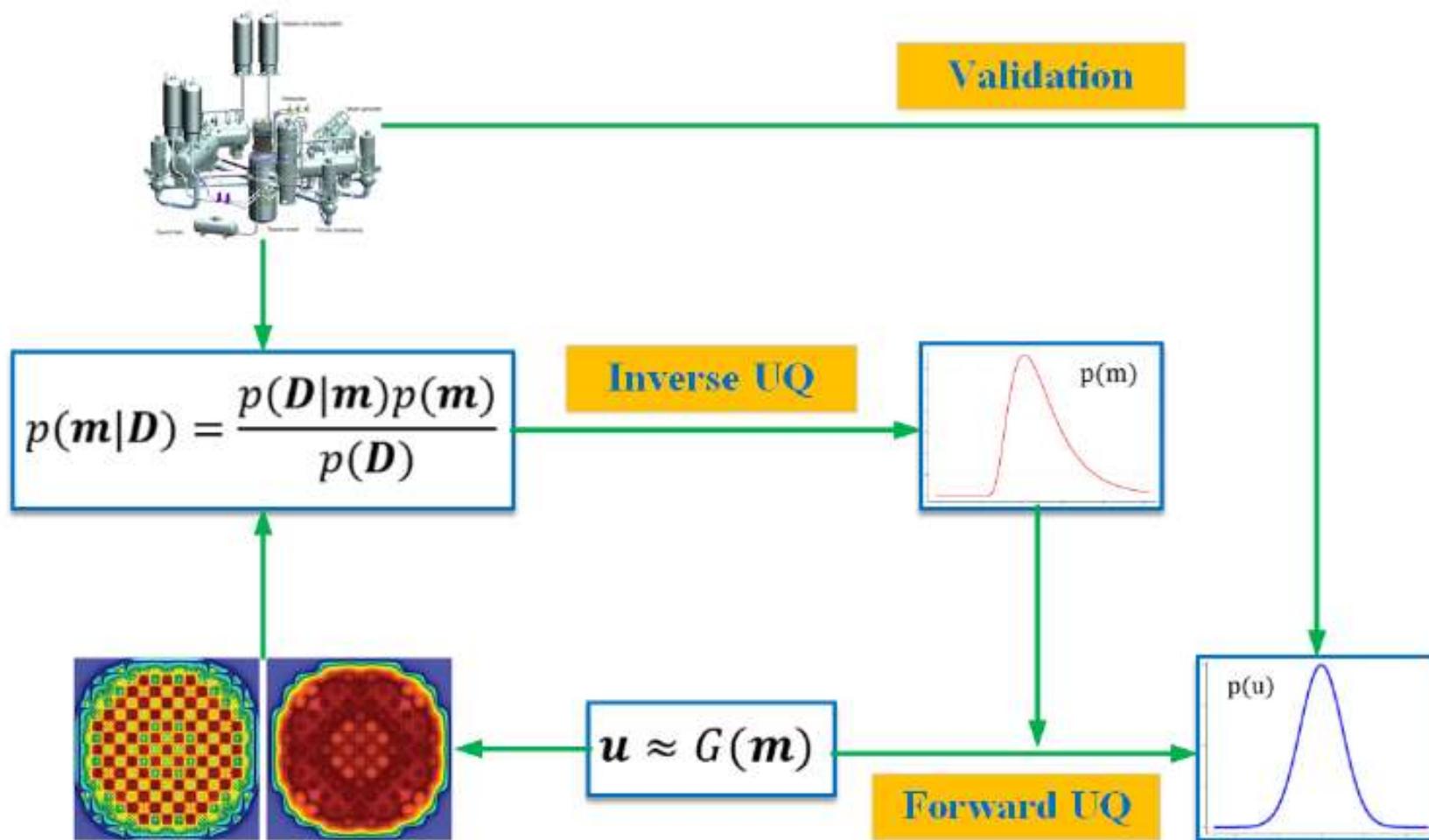
So what was it all about?



So what was it all about?







Forward vs Inverse Uncertainty Quantification

